

Treatment of Exposed Epoxy-Coated Reinforcement in Repair

Keywords: coating; corrosion; corrosion inhibitor; electrical resistance; reinforcing bars; epoxy-coated; reinforcing steel; repair; ring corrosion; sacrificial anode.

Introduction

 When epoxy-coated steel reinforcement is exposed in a repair area, the exposed reinforcement requires treatment prior to repair material placement.

Question

When epoxy-coated steel reinforcement is exposed in a repair area, how should the reinforcement be treated before placing the concrete repair?

Significance

The repair of structures containing epoxy-coated steel reinforcement presents issues that differ from structures containing uncoated steel reinforcement.

Answer

The coated steel should be treated to avoid creating corrosion cells that may result in accelerated corrosion of the reinforcement.

Discussion

During concrete removal and preparation of the repair area, the epoxy coating on the bars within the repair will be damaged, may already have defects or, as part of the repair procedure, be completely removed. Measures should be considered to avoid or minimize the risk of accelerated corrosion.

It is common practice to clean, prepare, and re-coat any exposed epoxy-coated steel reinforcement during the repair process, usually with an epoxy coating compatible with the existing fused coating on the steel. Additional protection should be considered because of the difficulty to re-coat the steel completely. Areas left uncoated (defects) may result in corrosion problems after the repairs are completed.

 When a concrete repair is undertaken, chloride-contaminated or carbonated concrete is typically removed and replaced with repair material. In many cases, not all of the contaminated concrete is removed. After the repair, the reinforcing steel may be in contact with concrete outside the repair area having varying levels of contamination. The differences in pH levels and in chloride ion concentrations between the new repair materials and the remaining contaminated concrete will result in differing corrosion potentials or voltages through the length of the reinforcing bar. A current will flow as a result of these voltage differences, leading to corrosion.

Reinforcement locations surrounded by concrete with the highest moisture and chloride contamination are likely to corrode first. Corrosion will occur in locations where there is both a defect in the coating and a sufficient level of contamination present. In general, the corrosion rate is proportional to the ratio of the cathodic area to the anodic area. Because the amount of coated steel is often far greater than the exposed steel, the rate of corrosion of the exposed steel can be extremely high. Additionally, the repaired area increases the cathodic (protected) area. As a result, corrosion of the steel immediately adjacent to the repair area at locations with defects or where the epoxy has delaminated will continue, and the rate may even accelerate. The uncoated area of steel inside the repair area will contribute toward the overall corrosion cell, which could result in corrosion of steel in the existing concrete in the locations where sufficient contamination, oxygen, and moisture are present. It is also possible that corrosion will occur within the patch by current flow between any re-coated epoxy coating defects.

In addition to coatings, other options exist to address these issues. They include the use of noncorrosive reinforcement, metallic coatings for steel reinforcement (both sacrificial or noble and nonsacrificial types), chemical inhibitors, and cathodic protection systems (both impressed current and galvanic types), which are

discussed elsewhere (ACI 222R; ICRI 310.R). It is recommended that supplemental corrosion protection be provided for existing steel reinforcement by coating the reinforcing bar using either a high-electrical-resistance repair concrete that may contain an appropriate inhibitor, embedded galvanic anodes, or both, as illustrated in Table 1. A combination of corrosion protection methods from Table 1 will usually provide better corrosion protection than any individual method.

Summary

 The use of coatings can be beneficial in reducing the surface area of steel available to promote corrosion. The use of high-electrical-resistance repair materials can reduce the corrosion current by increasing the circuit resistance. The use of repair materials that contain inhibitors can be beneficial if the type of inhibitor used increases the circuit resistance. The use of embedded galvanic anodes can be beneficial in providing galvanic corrosion protection to portions of the steel where the epoxy coating is defective, either inside or adjacent to the repair. Treating exposed epoxy-coated reinforcing in repair areas is recommended to suppress ongoing corrosion activity.

Referenced standards and reports

 The standards and reports listed below were the latest editions at the time this document was prepared. Because these documents are revised frequently, the reader is advised to contact the proper sponsoring group if it is desired to refer to the latest version.

American Concrete Institute

Protection of Metals in Concrete Against Corrosion

International Concrete Repair Institute

310.R Guideline for Surface Preparation for the Repair of Deteriorated Concrete Resulting from Rein forcing Steel Corrosion (formerly No. 03730)

These publications may be obtained from these organizations: American Concrete Institute 38800 Country Club Drive Farmington Hills, MI 48331 www.concrete.org

International Concrete Repair Institute 10600 West Higgins Road, Suite 607 Rosemont, IL 60018 www.icri.org

Reported by ACI Committee 364

Fred R. Goodwin Chair

Majorie M. Lynch Secretary

Randall M. Beard Benoit Bissonnette Christopher D. Brown Douglas Burke Ryan Alexander Carris Bruce A. Collins Brian Lee Cope Boris Dragunsky Peter H. Emmons Paul E. Gaudette Timothy R. W. Gillespie Zareh B. Gregorian Pawan R. Gupta John L. Hausfeld

Ron Heffron Robert L. Henry Kal R. Hindo Charles J. Hookham Ashok M. Kakade Dov Kaminetzky James M. Kasper Emory L. Kemp Keith E. Kesner Erick N. Larson Majorie M. Lynch Pritpal S. Mangat Surendra K. Manjrekar

James E. McDonald William R. Nash Jay H. Paul K. Nam Shiu Thomas E. Spencer John A. Tanner Valery Tokar David A. VanOcker Alexander M. Vaysburd Kurt F. von Fay James Warner Patrick M. Watson David W. Whitmore

ACI TechNotes are intended for reference for the design and construction of concrete structures. This document is intended for the use of individuals who are competent to evaluate the significance and limitations of its content and who will accept responsibility for the application of the information it contains. The American Concrete Institute disclaims any and all responsibility for the accuracy of the content and shall not be liable for any loss or damage arising therefrom. Reference to this document shall not be made in contract documents.

ACI 364.3T-10 was adopted and published January 2010.

Copyright © 2010, American Concrete Institute.

All rights reserved including the rights of reproduction and use in any form or by any means, including the making of copies by any photo process, or by electronic or mechanical device, printed, written, or oral, or recording for sound or visual reproduction or for use in any knowledge or retrieval system or device, unless permission in writing is obtained from the copyright proprietors.

For additional copies, please contact: American Concrete Institute, 38800 Country Club Drive, Farmington Hills, MI 48331 Phone: 248-848-3700 Fax: 348-848-3701 www.concrete.org