



Post-Earthquake Repairs, Part 2

ACI Spring 2012 Convention
March 18 – 21, Dallas, TX



Murat Saatcioglu is a Distinguished University Professor and University Research Chair in the Department of Civil Engineering of the University of Ottawa, Ottawa, Canada. He is the Director of the Hazard Mitigation and Disaster Management Research Centre of the same university. He has conducted extensive experimental and analytical research on earthquake resistant concrete structures, including the development of seismic design and retrofit methodologies for reinforced concrete and masonry structures. Professor Saatcioglu is the recipient of numerous research and teaching awards, including the Wason Medal from the American Concrete Institute in 2004, the Raymond C. Reese Research Prize from the American Society of Civil Engineers in 2000, Casimir Gzowski Medal from the Canadian Society for Civil Engineering in 2001 and 2004, CCEDS-1 Award for Best Paper from McMaster University in 2005. He is a Fellow of the American Concrete Institute.



Seismic Repair of Reinforced Concrete Columns through Transverse Prestressing

Murat Saatcioglu
Department of Civil Engineering
University of Ottawa
Ottawa, CANADA

Majid Yarandi
Imperial Oil Resources
Calgary, CANADA



Potential Failure Modes in Columns

- Shear
- Compression
- Crushing
- Splice Failure



Repair and Retrofit through External Prestressing



- RetroBelt is a system of external prestressing concrete columns in transverse direction.
- Lateral force exerted by RetroBelt controls diagonal tension cracks while providing shear reinforcement, improving shear capacity.
- Lateral pressure exerted by RetroBelt, both active and passive, confines concrete and improves bond in splice regions, enhancing column ductility.



External Prestressing





 **uOttawa External Prestressing**




1
2
3
4



 **uOttawa External Prestressing**





BR-C7
1%



 **uOttawa External Prestressing**




 **uOttawa Corrosion Protection**






BR-SP2
1%


7%

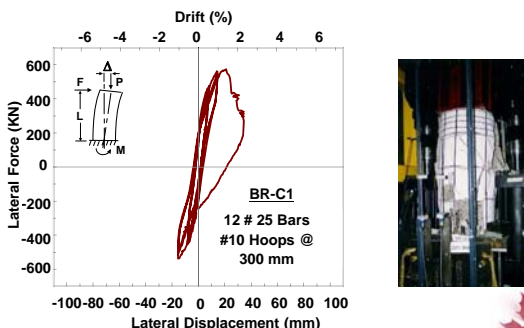
BR-SP2



 **uOttawa Field Application**



 **uOttawa Shear Deficient Circular Column**




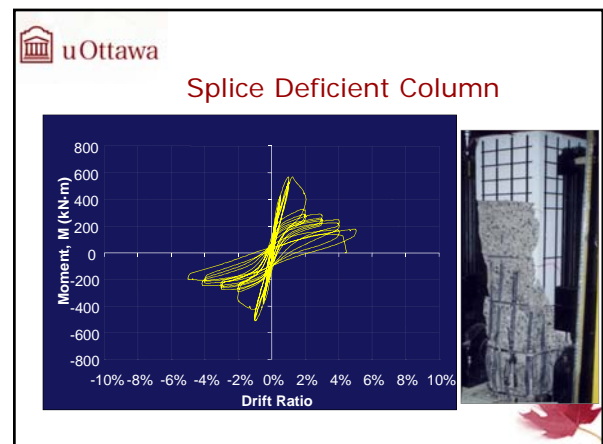
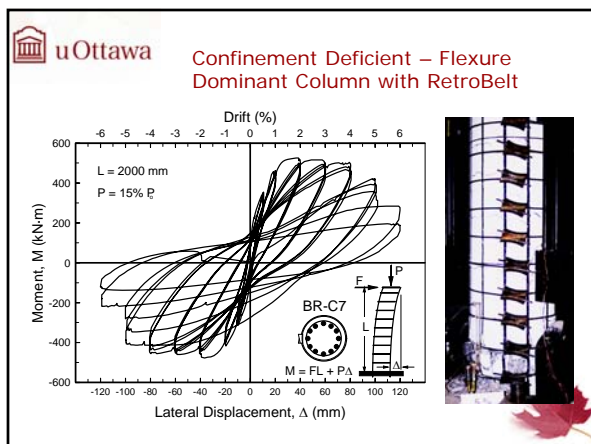
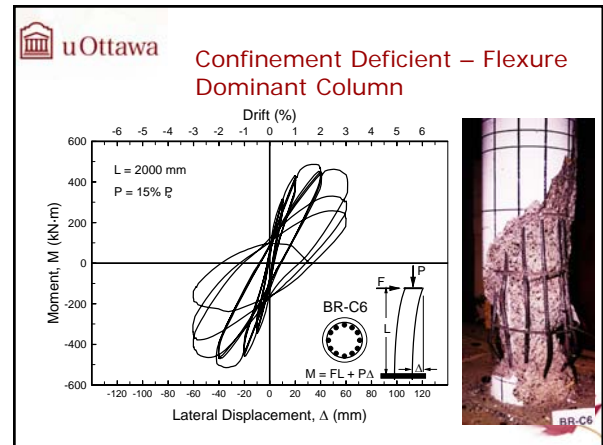
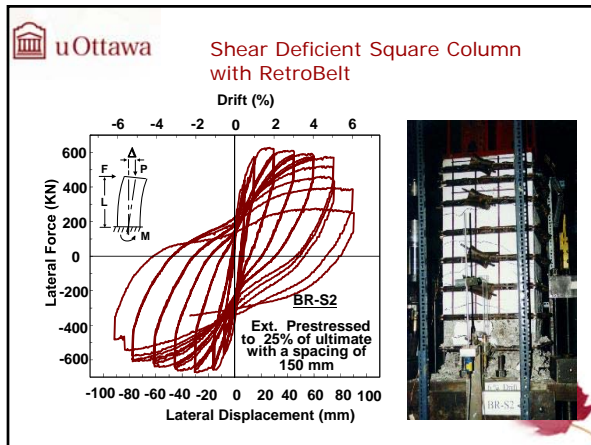
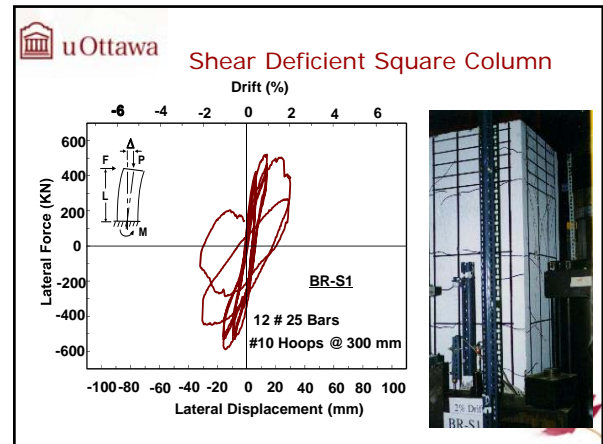
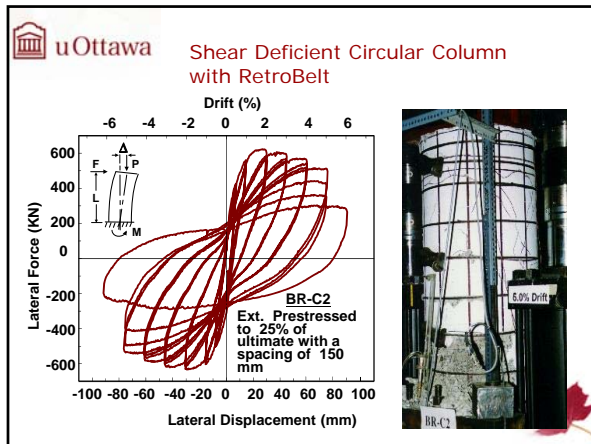
Drift (%)

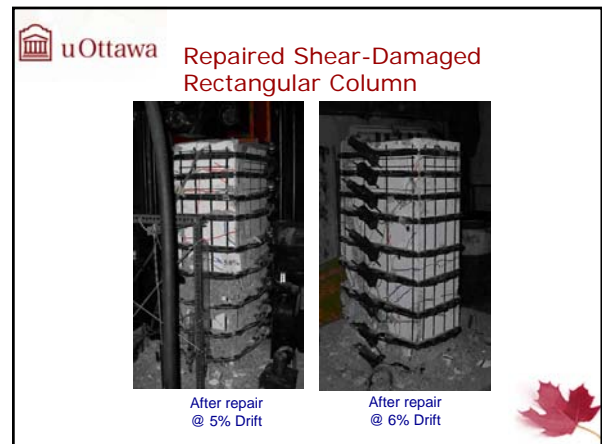
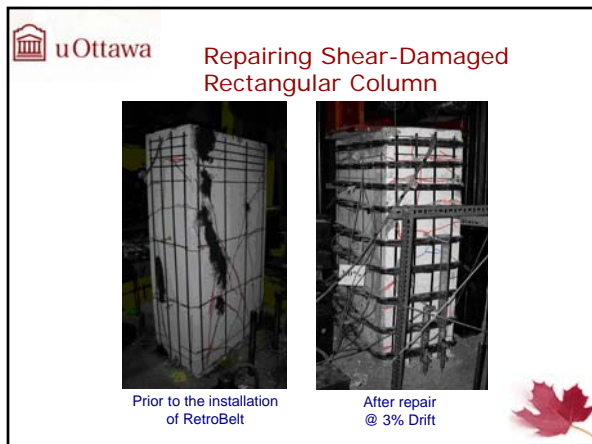
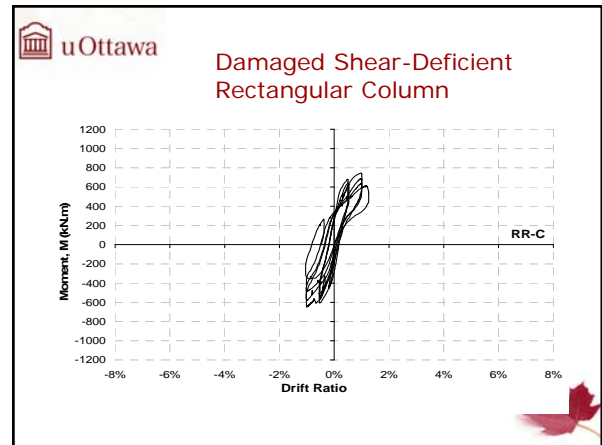
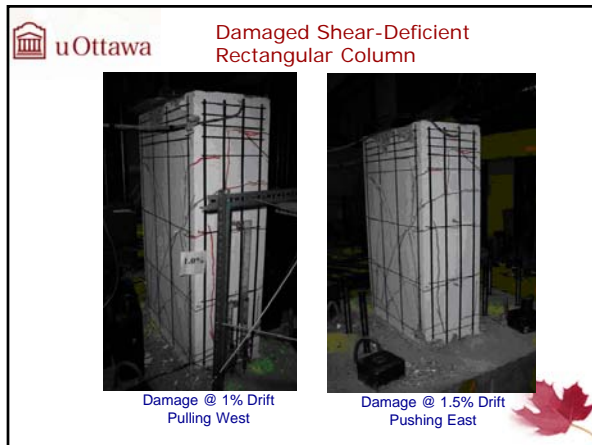
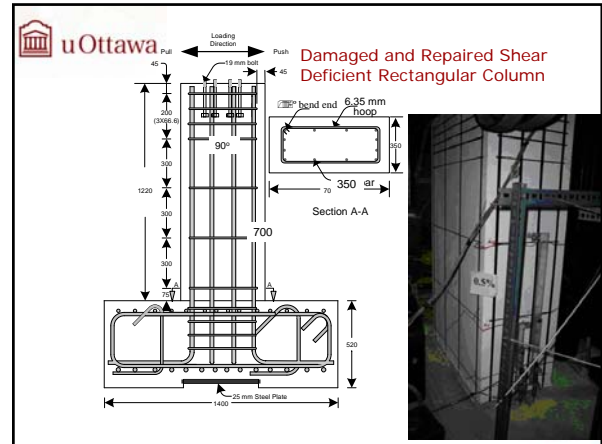
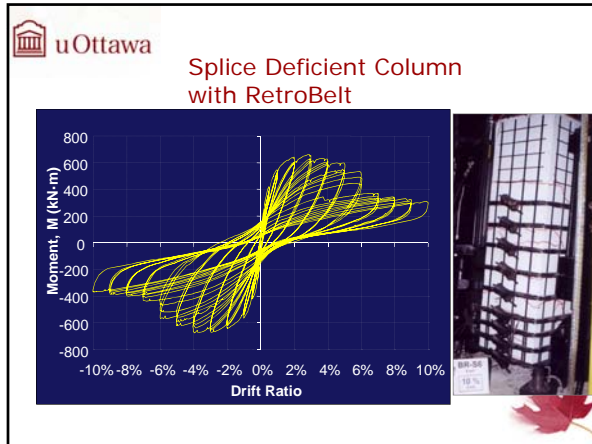
Lateral Force (kN)

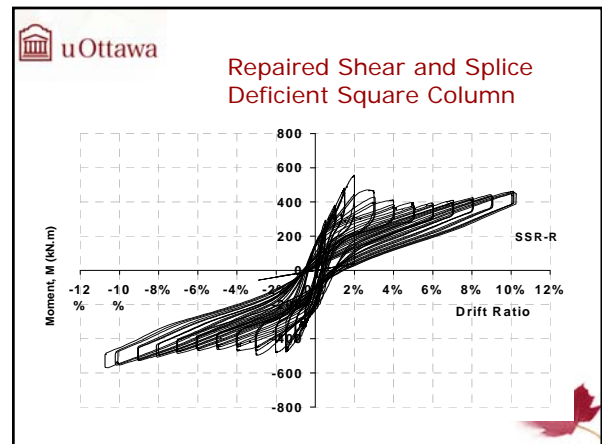
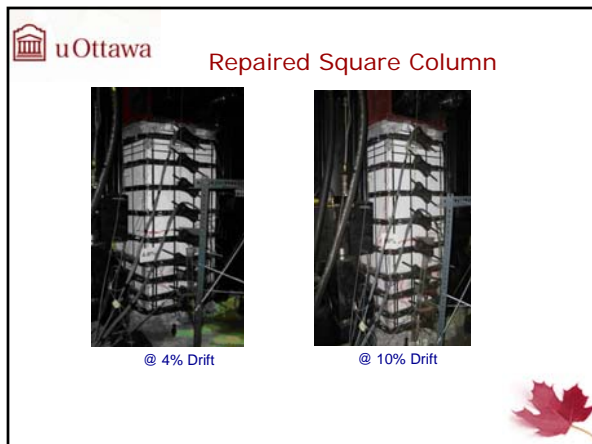
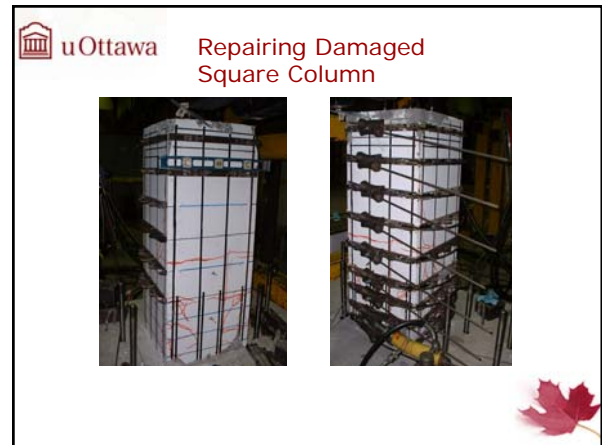
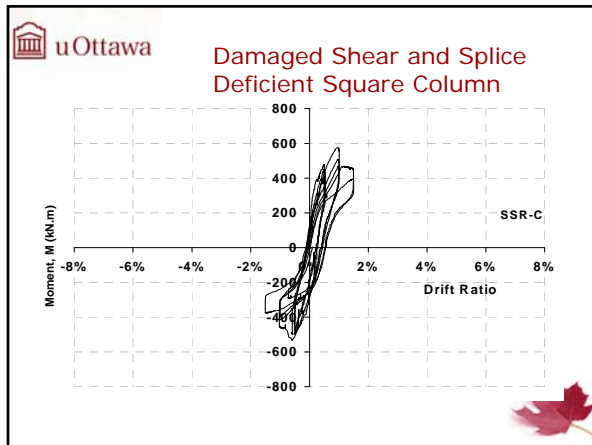
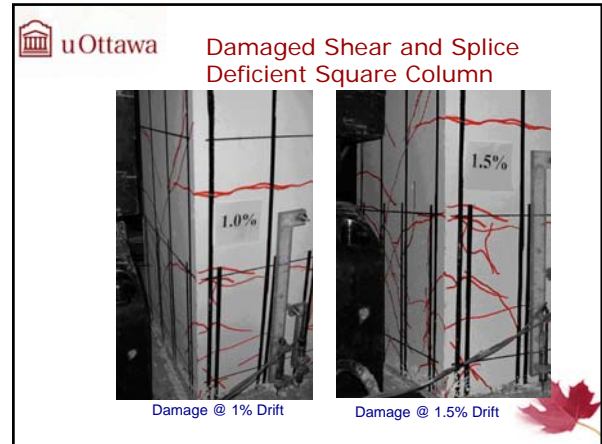
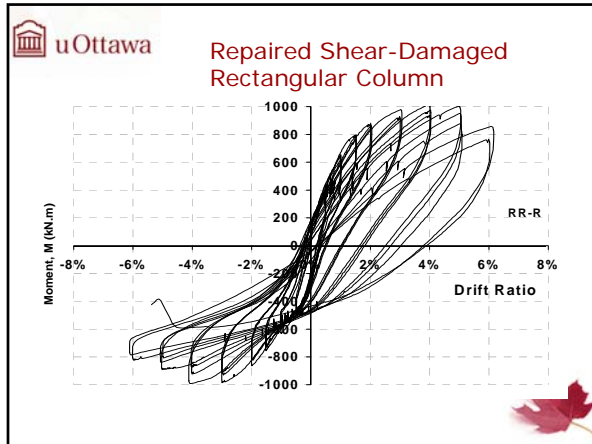
Lateral Displacement (mm)

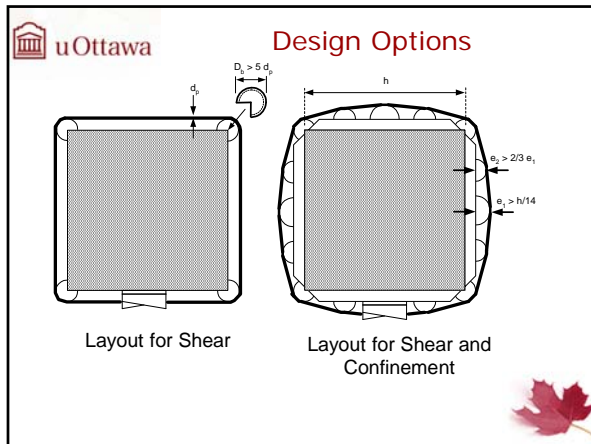
BR-C1
12 # 25 Bars
#10 Hoops @
300 mm












 uOttawa


Shear Design


$$V_n = V_c + V_s + V_p$$

Contribution of prestressing to concrete shear capacity:

$$V_{pc} = 2A_{pc} f_{pi} \frac{h}{s_p}$$

Additional shear reinforcement:

$$V_{ps} = 2A_{ps} (f_{py} - f_{pi}) \frac{h}{s_p}$$


 uOttawa


Repair and Retrofit for Concrete Confinement


$$\rho_c = 14 \frac{f'_c}{f_{yh}} \left[\frac{A_g}{A_c} - 1 \right] \frac{1}{\sqrt{k_c}} \frac{P}{\phi P_0} \delta$$

$$A_{ps} = 2 \frac{f'_c}{f_{pe}} \frac{P}{\phi P_0} h s_{ps} \delta$$

$$f_{pe} = f_{pi} + 0.003 E_p$$

↑ 0.001 E_p for splice clamping



 uOttawa

Conclusions

Thank You...

Questions or Comments?

