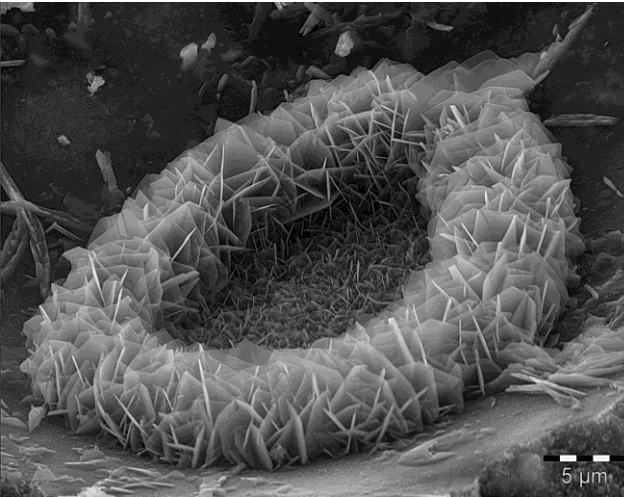


# Influence of Pumping on Fresh Concrete Properties for SCC



***Thomas A. BIER – Keisuke TAKAHASHI***

- Earlier Experiences
  - Field Trials
  - Literature on Mixing
- Materials and Testing
- Macrolevel
  - Influence on rheological Properties and workability
- Microlevel
  - Hydration, Chemistry and Microstructure
- Concept and Summary
- Conclusions

# Abstract



During field trials, involving pumping of self compacting concrete, changes in rheological properties have been observed. In order to predict possible changes, studies were undertaken on self compacting mortar (SCM) where various mixing as well as pumping intensities were applied. As a result not only changes in rheological properties but also changes in hydration kinetics were observed. It has been shown that mixing and shear stress during pumping, respectively, do exhibit a pronounced influence on rheological properties of self-compacting mortars. The changes in rheological properties can be explained by the dispersion of the particles as well as an accelerated formation of pre-hydrates during early hydration.



# Process Chain Underground Pumping

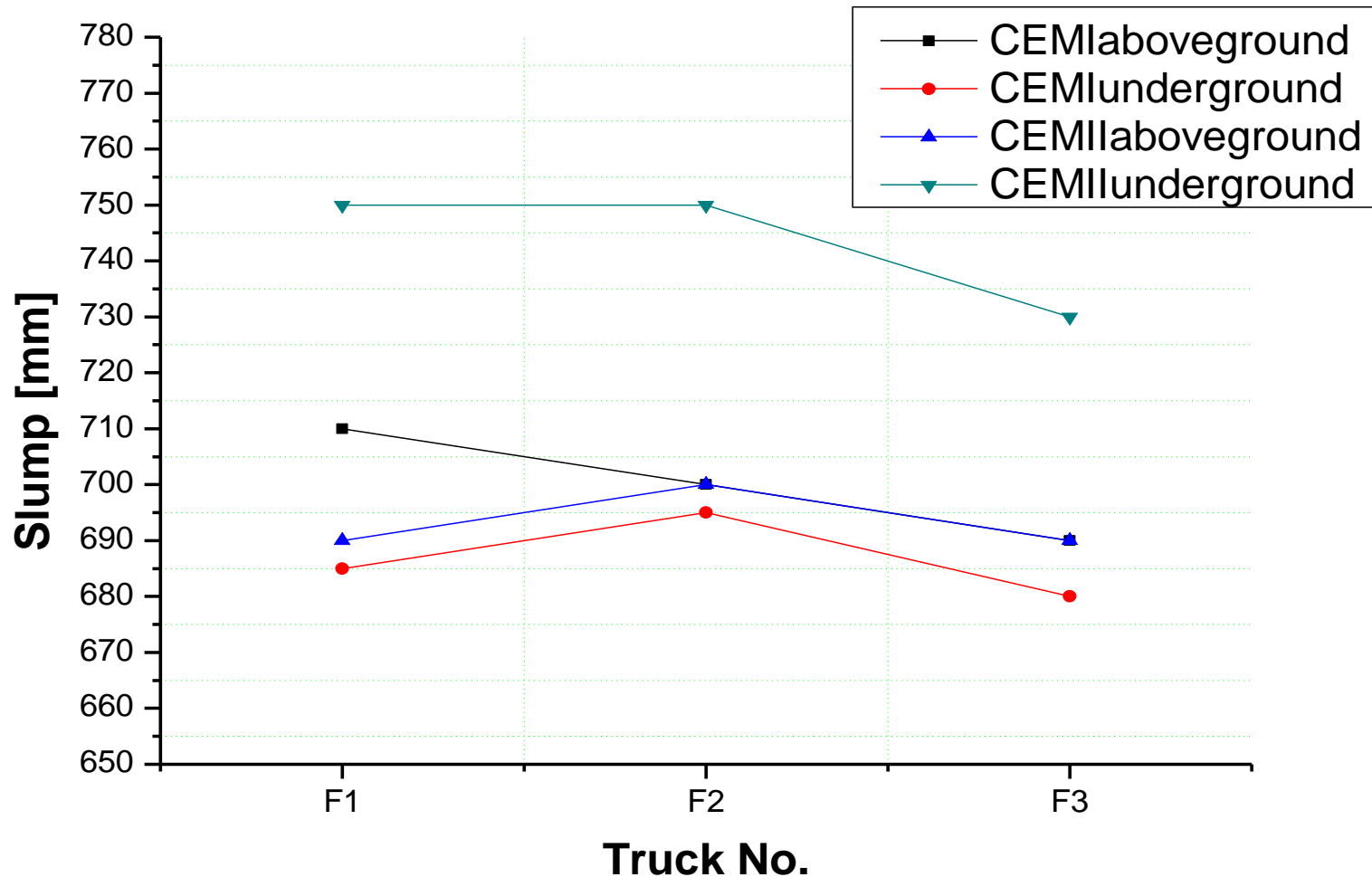




# Process Chain Underground Pumping

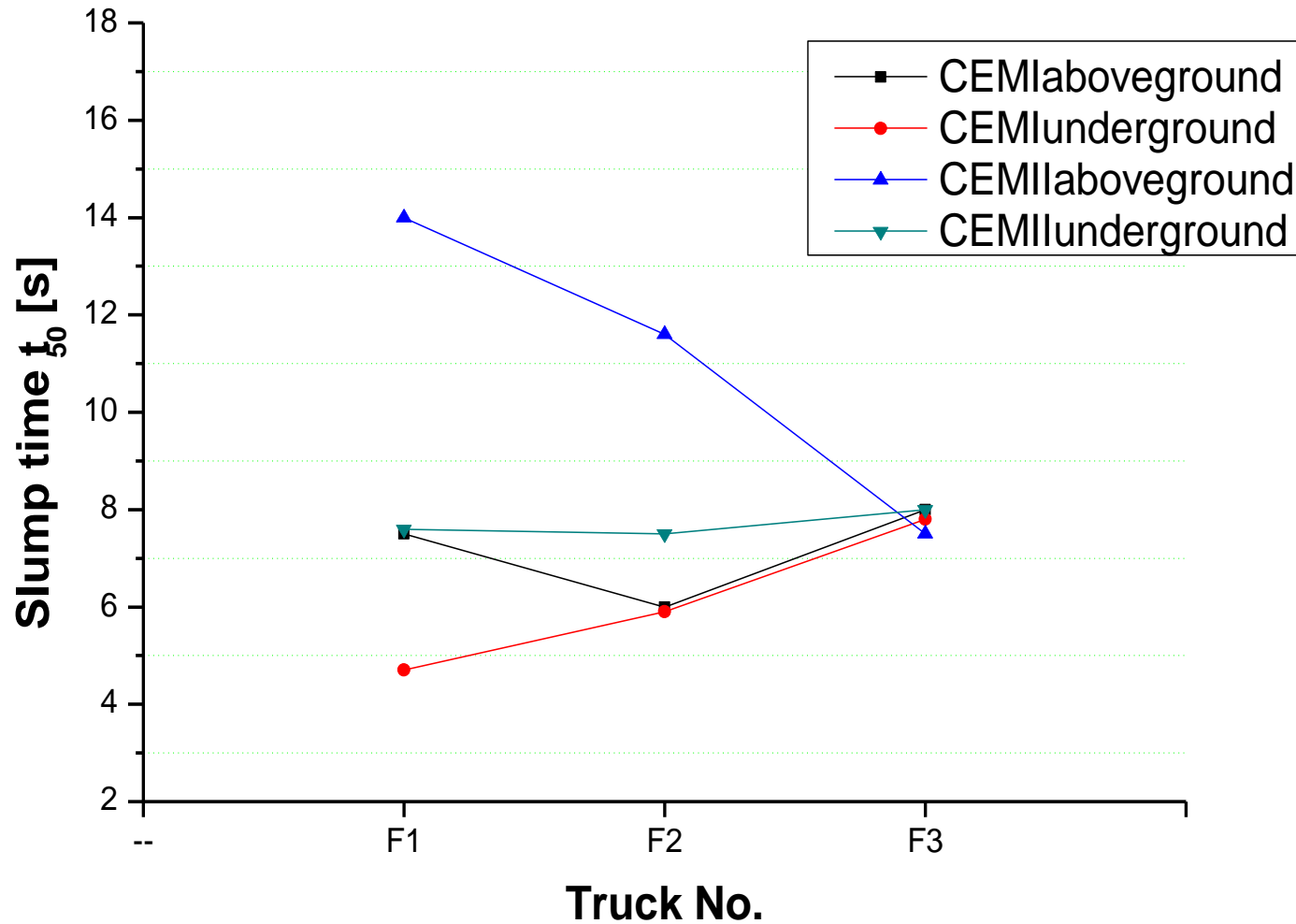


# Slump Flow Value



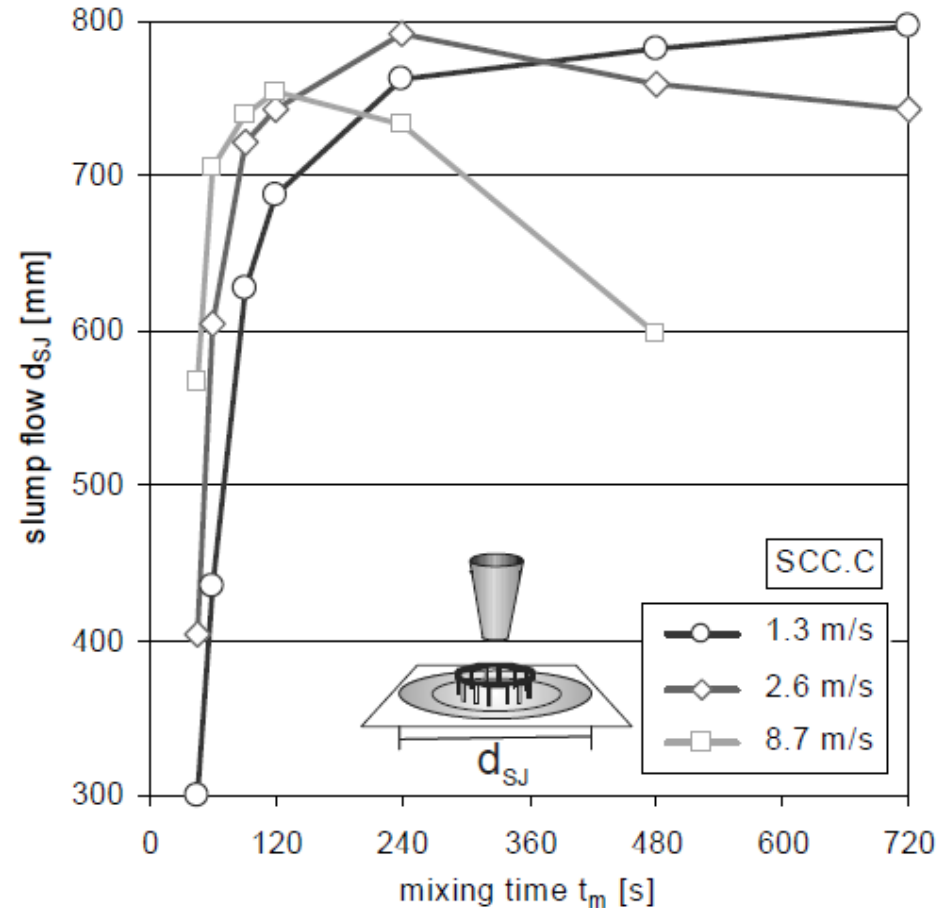
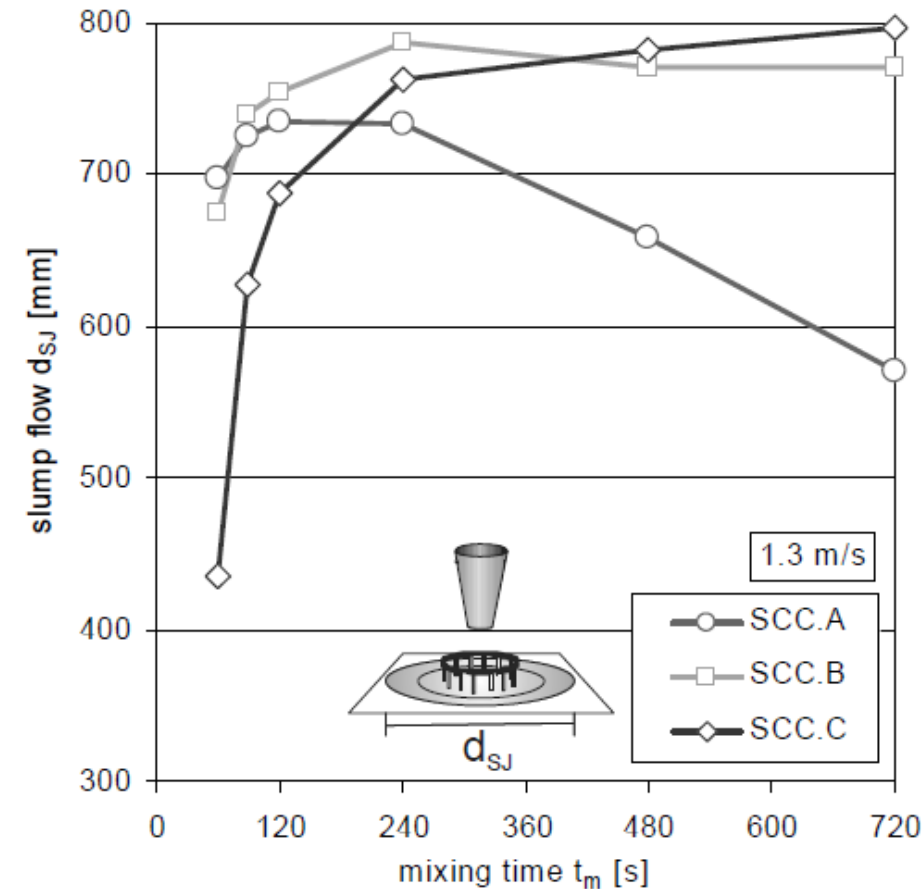
*Self Compacting Concrete Underground ; Dahlhaus, Bier et. al, Ibausil, 2006*

# Slump Flow Time



*Self Compacting Concrete Underground ; Dahlhaus, Bier et. al, Ibausil, 2006*

# Mixing time and mixing speed



**Optimum mixing time: SCC. B is longer than SCC. A**

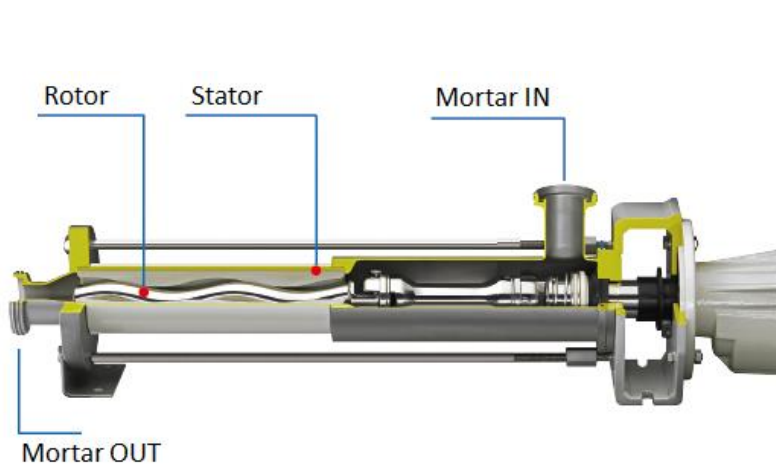
**Chemical additive contents: SCC. C is higher than SCC. B**

*Lowke, D.; Schießl, P.: Effect of mixing energy on fresh properties of SCC in: Proceedings of the 4th International RILEM Symposium on Self-Compacting Concrete, Chicago, USA, 2005*

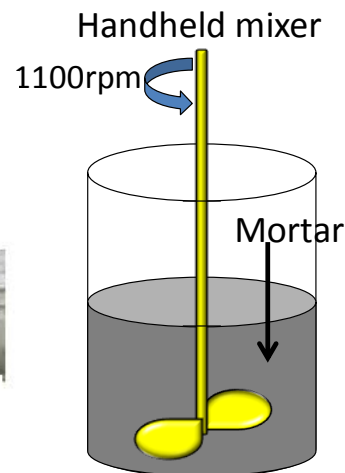


	Cement	Sand	PCE	HMC	Others*	Water
Grout	389	583	0.68	0.003	27.3	155
Cement paste	565	0	0.99	0	0	225

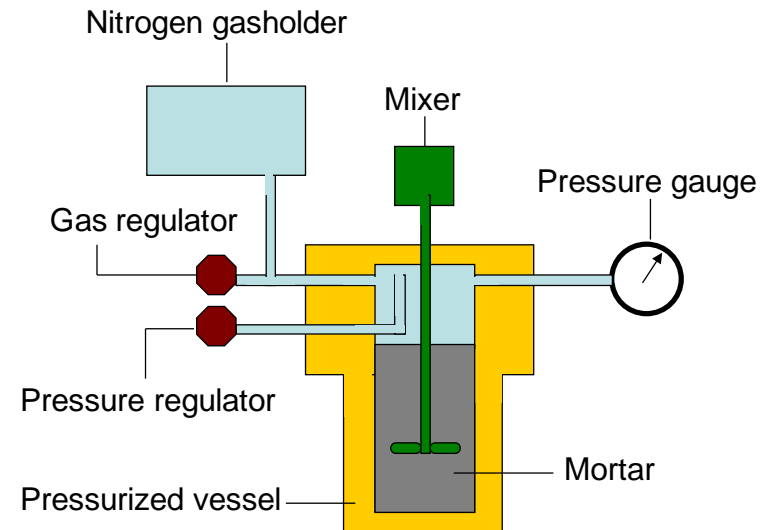
All tests were conducted at 20 °C using the same mortar mixed for 2 min.  
Measured pumping pressure was 2 MPa @ 50 m and 3 MPa @ 100 m.



Snake pump



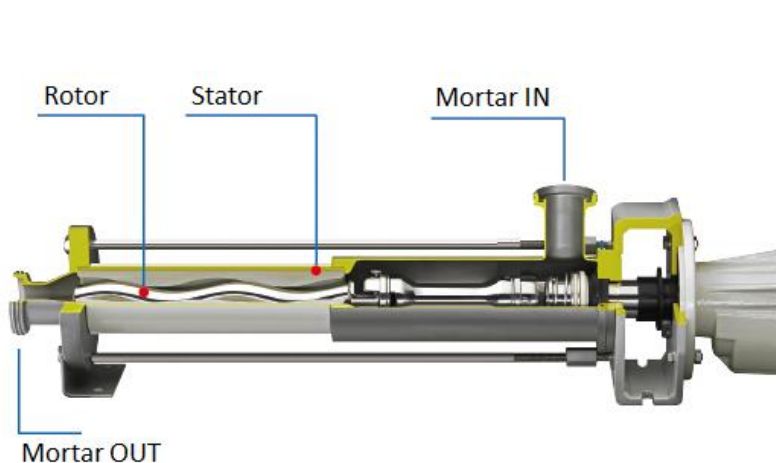
Handheld mixer



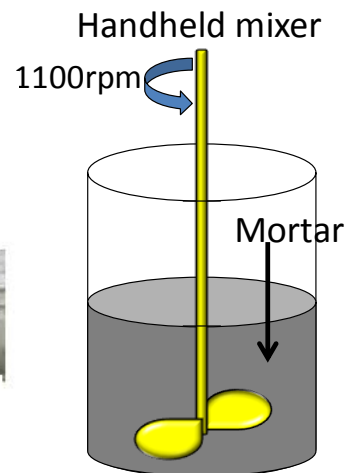
Pressurization apparatus

Factors	Pumping	Mixing	Pressurization	Sedimentation
Parameters	Pumping distances	Additional mixing periods	Pressure values	Sedimentation periods
	0, 50 and 100 m	0, 3 and 5 min	0, 2 and 3 MPa	0, 3 and 5 min

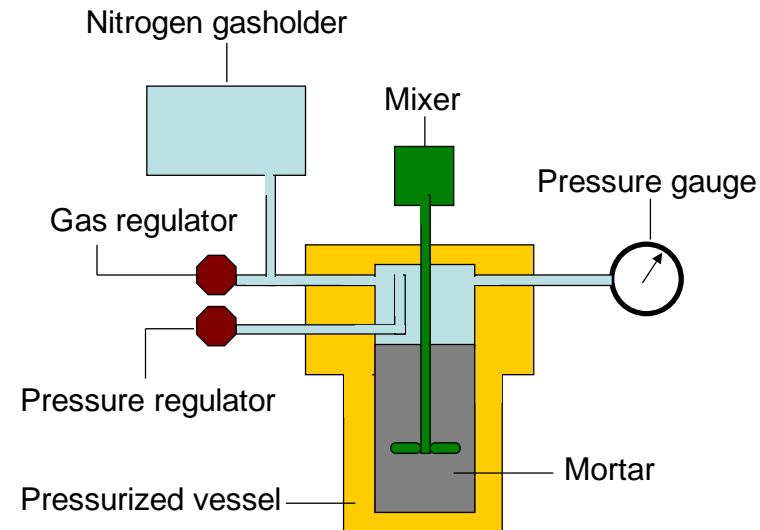
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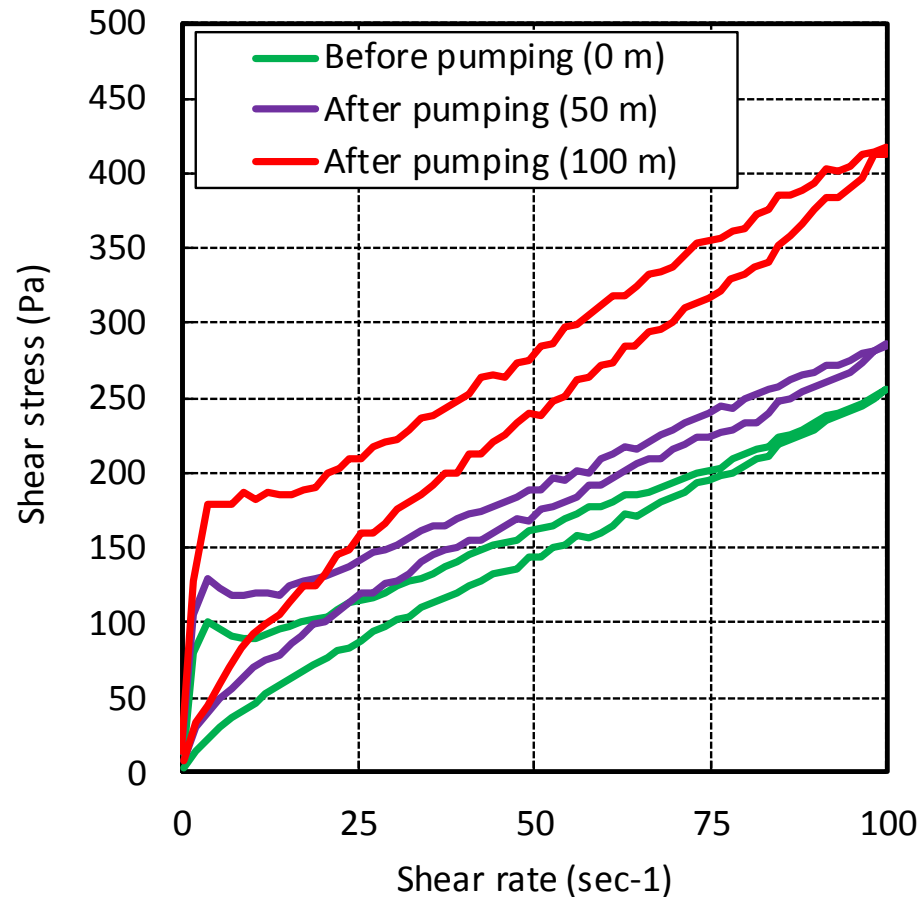
Handheld mixer



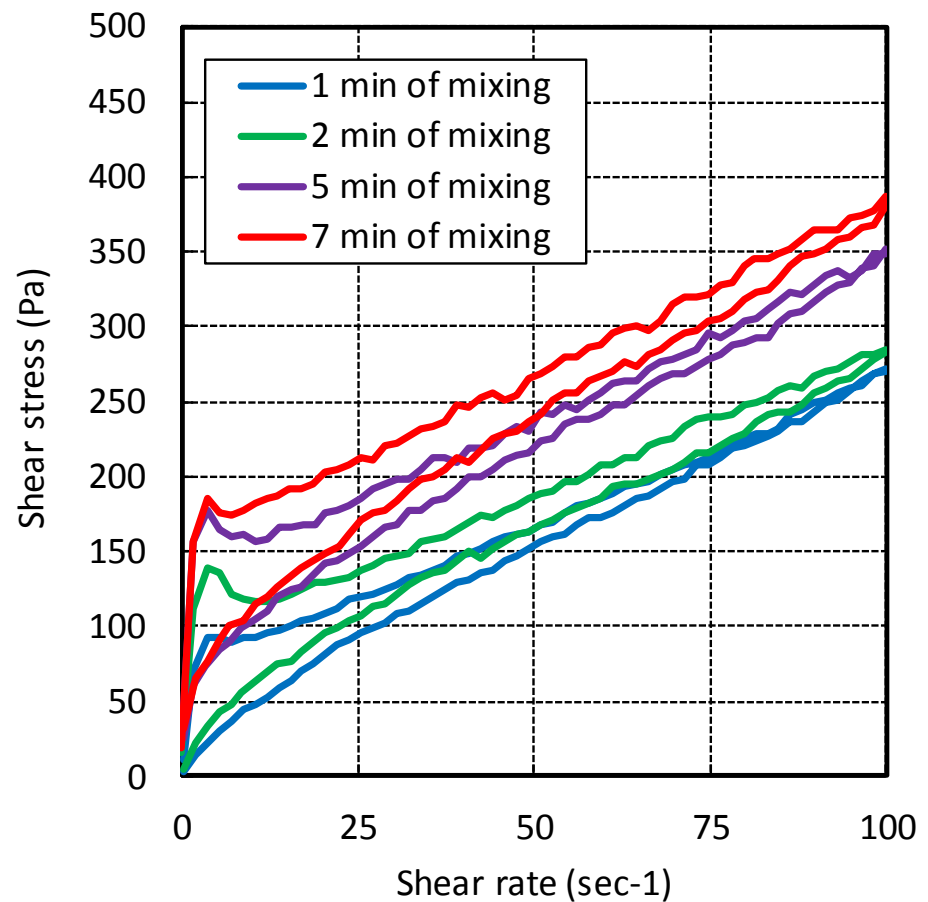
Pressurization apparatus

# Flow Curves

## Shear stress vs. shear rate



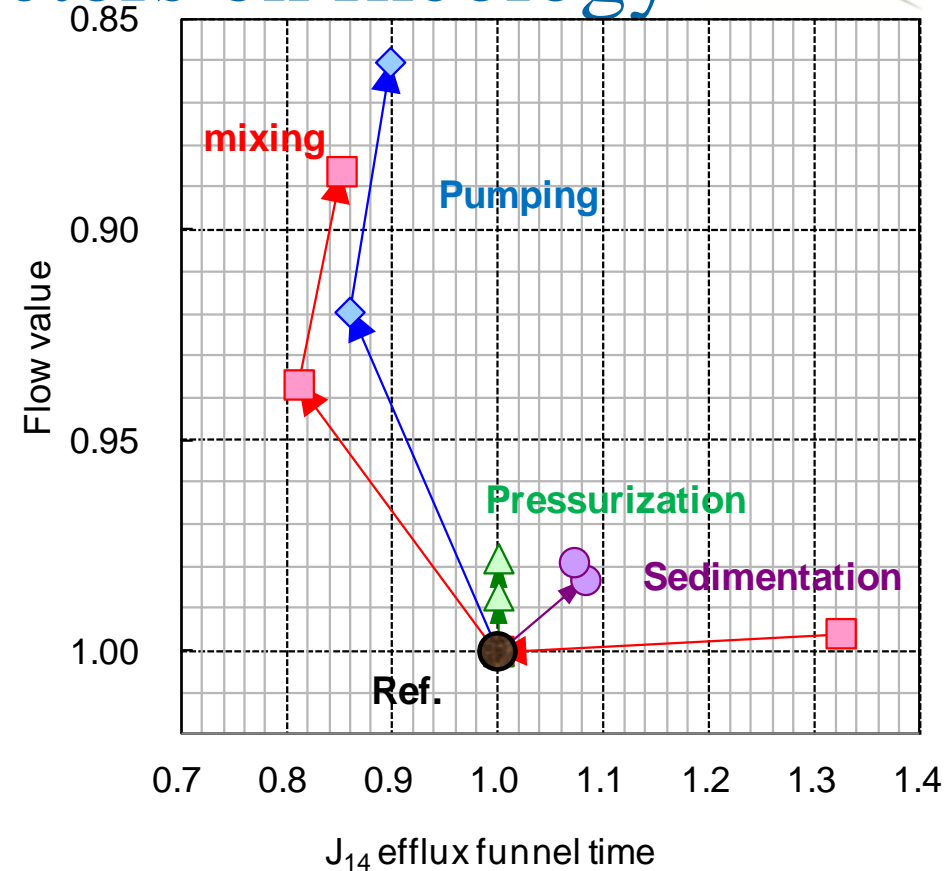
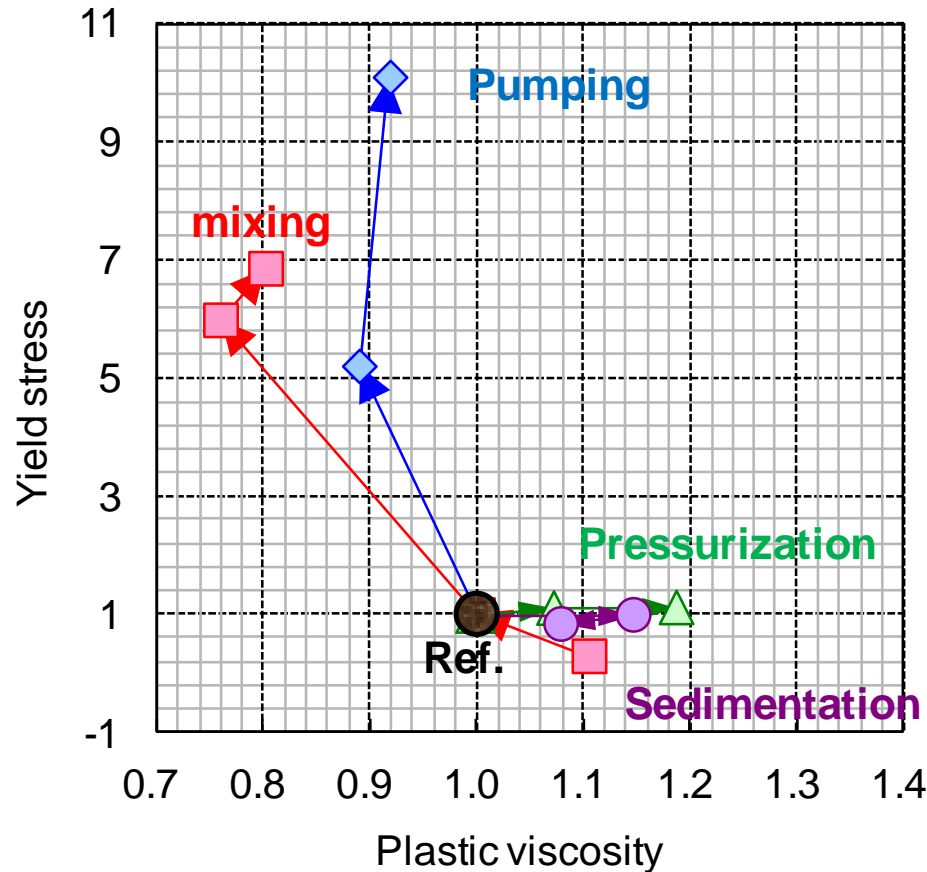
Pumping



Mixing



## Effects of several factors on rheology

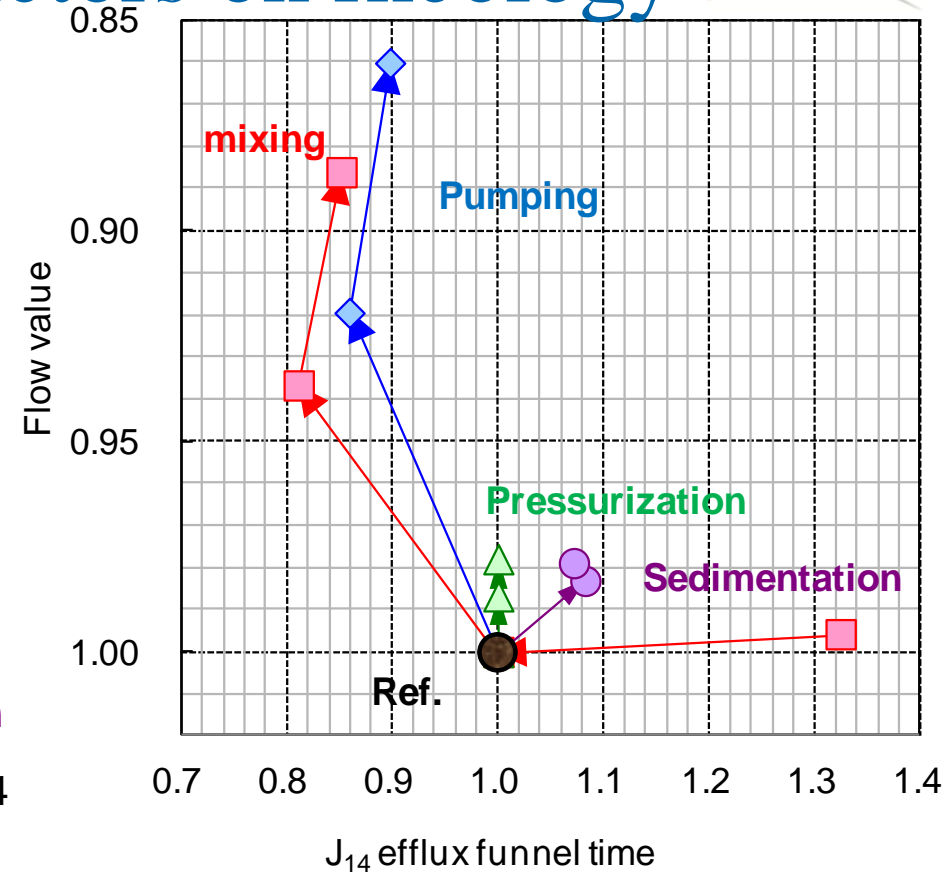
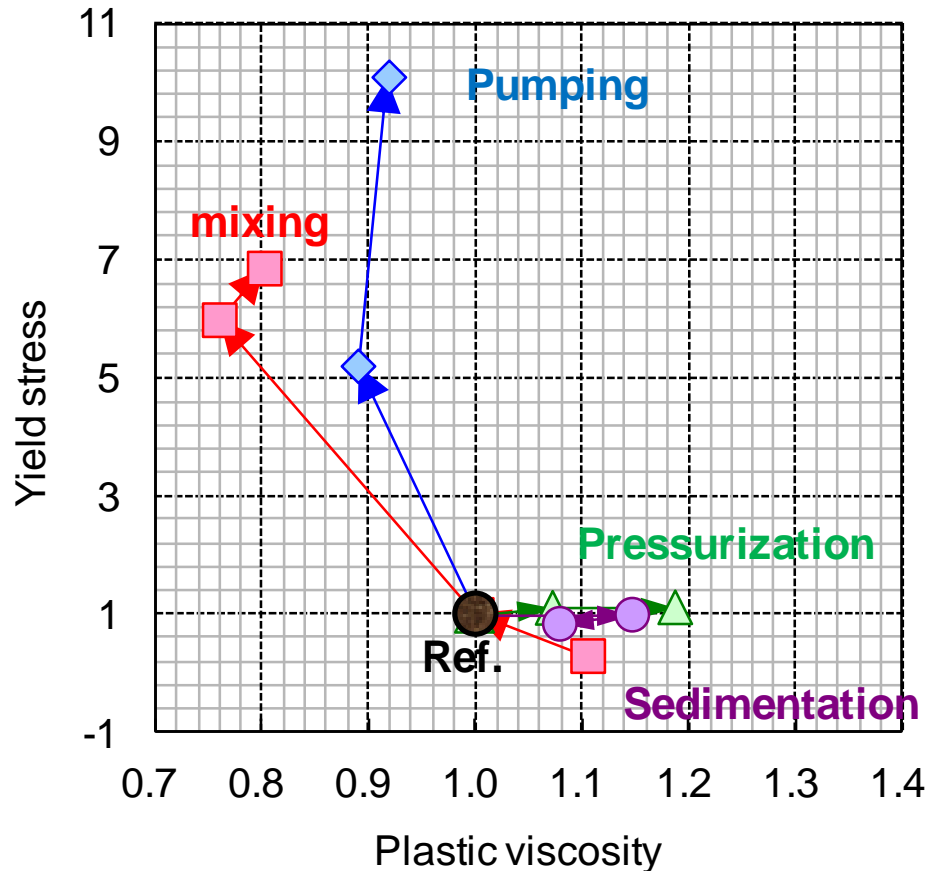


Reference point: after 2 min of mixing or before pumping

Mixing: 1→2→5→7 min, Pumping distances: before→after 50m→after 100m

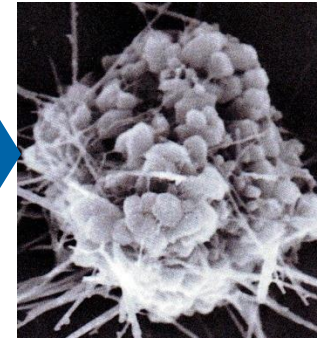
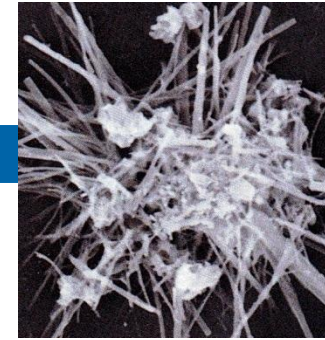
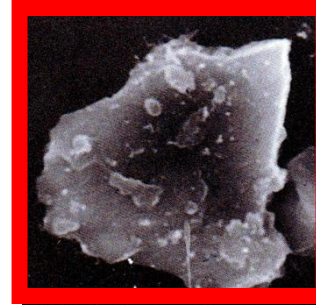
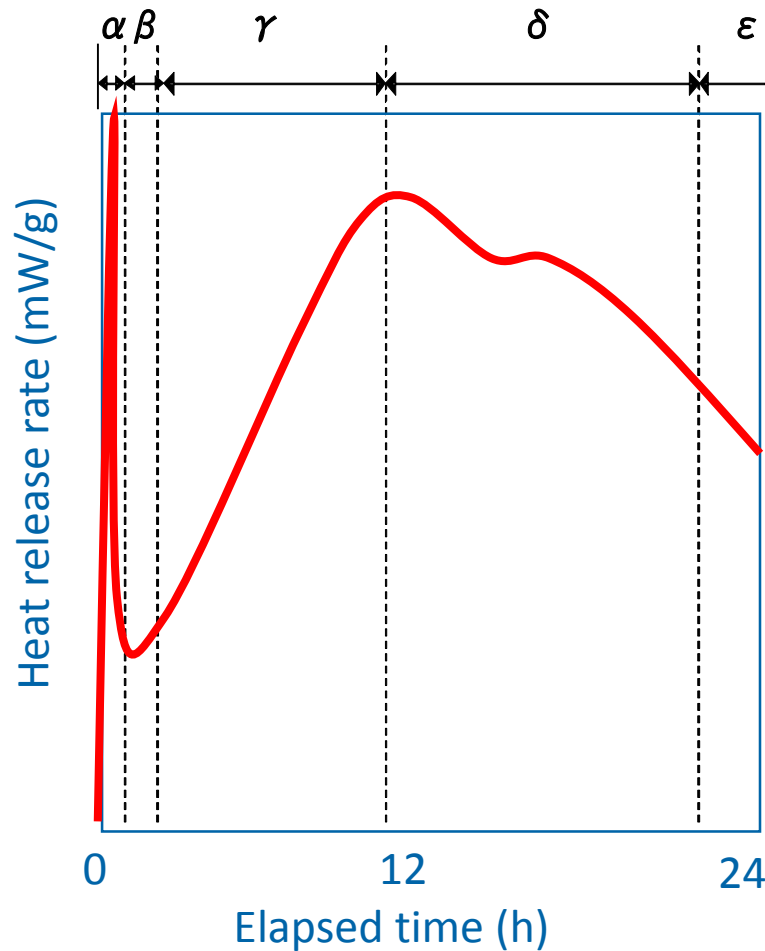
Pressurization: 0→2→3MPa, Sedimentation: 0→3→5 min

## Effects of several factors on rheology



- Shearing action during mixing and pumping process as well does exhibit the most pronounced effect
- Pressurization and sedimentation induce only little changes
- Efflux time and flow value correspond to viscosity and yield stress, respectively

# The early hydration process



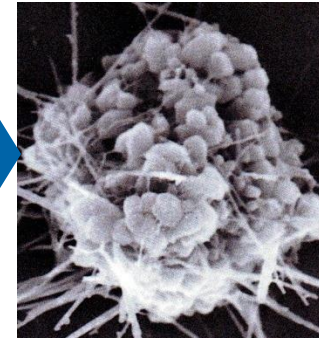
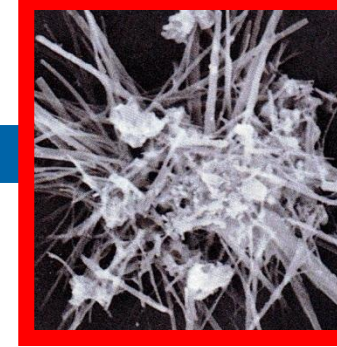
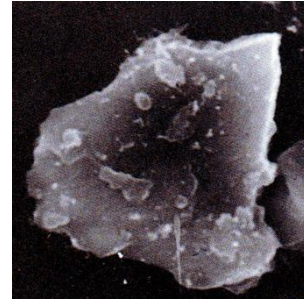
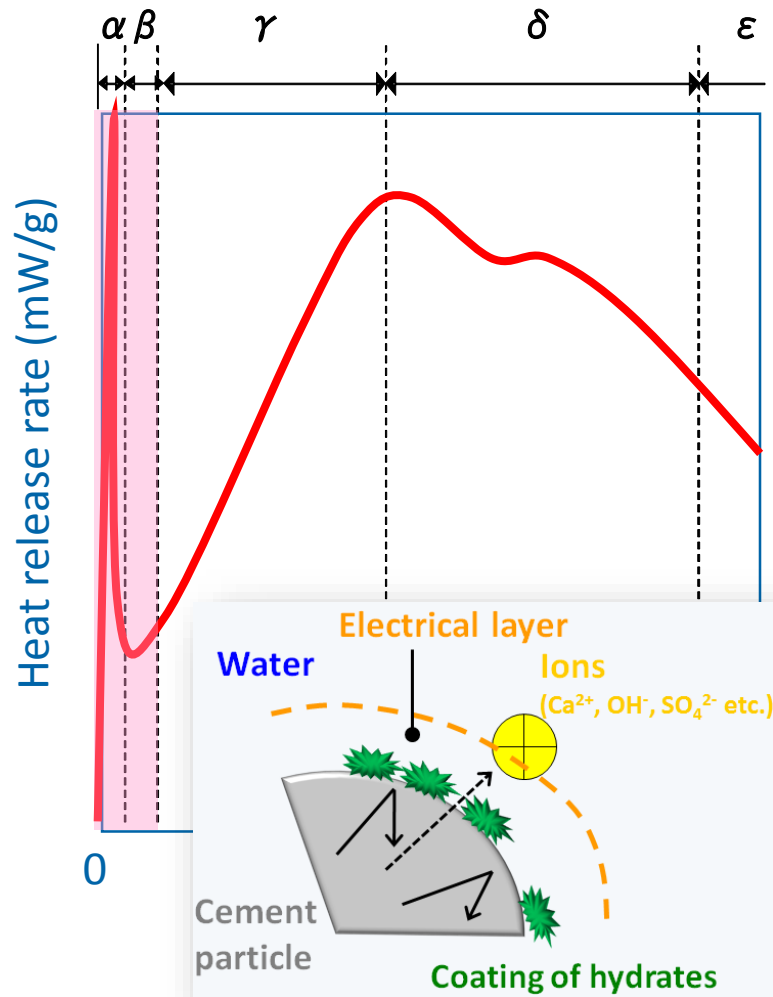
Hydration is

- exothermal reaction
- dissolution–precipitation process

Calorimetry curve for OPC paste



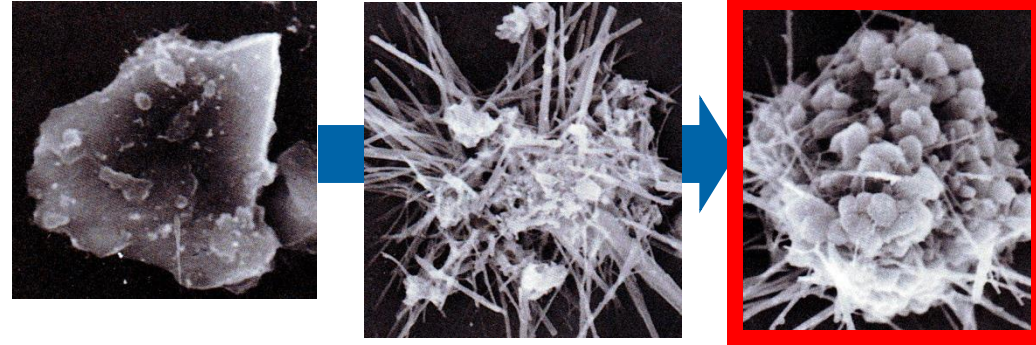
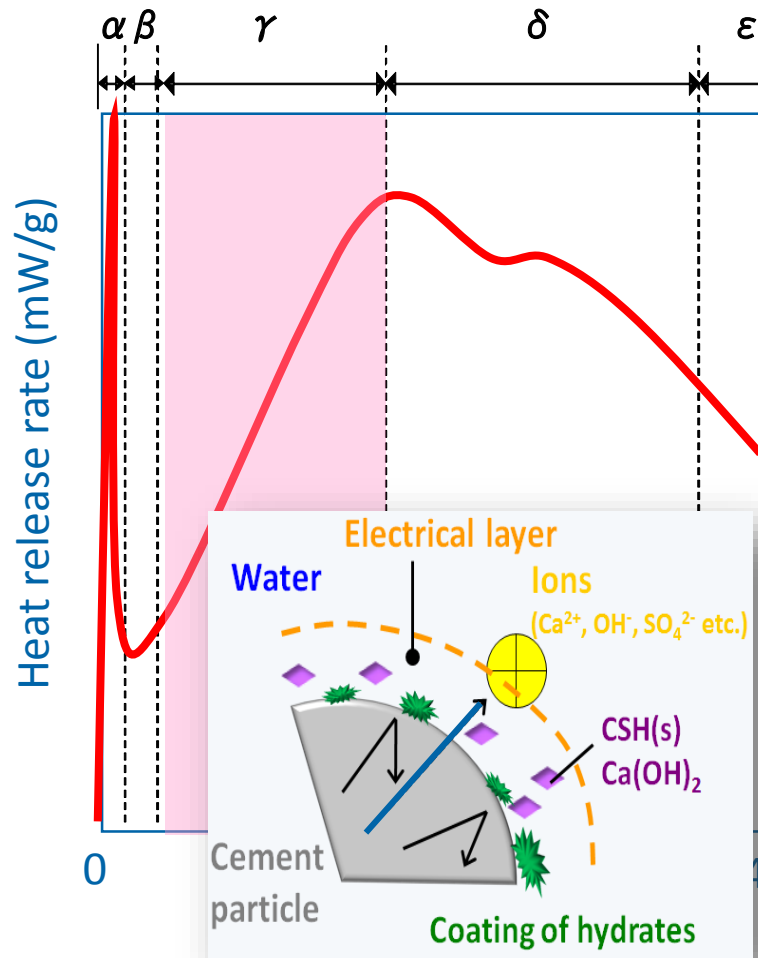
# The early hydration process



- Pre-induction (α) and induction (β) periods
- Initial dissolution and precipitation that provide a coating of hydrates (metastable layer, Stein, J. appl. Chem. 1964)
- $$\text{C}_3\text{S}, \text{C}_3\text{A} \xrightarrow{+\text{H}_2\text{O}} \text{CSH(m)}, \text{Ettringite}$$
- Set up of concentration gradient due to the increase of Ca<sup>2+</sup> at the interface (electrical layer, Juilland, CCR, 2010)
- The layers slow down the reaction rate

Calorimetry curve for OPC paste

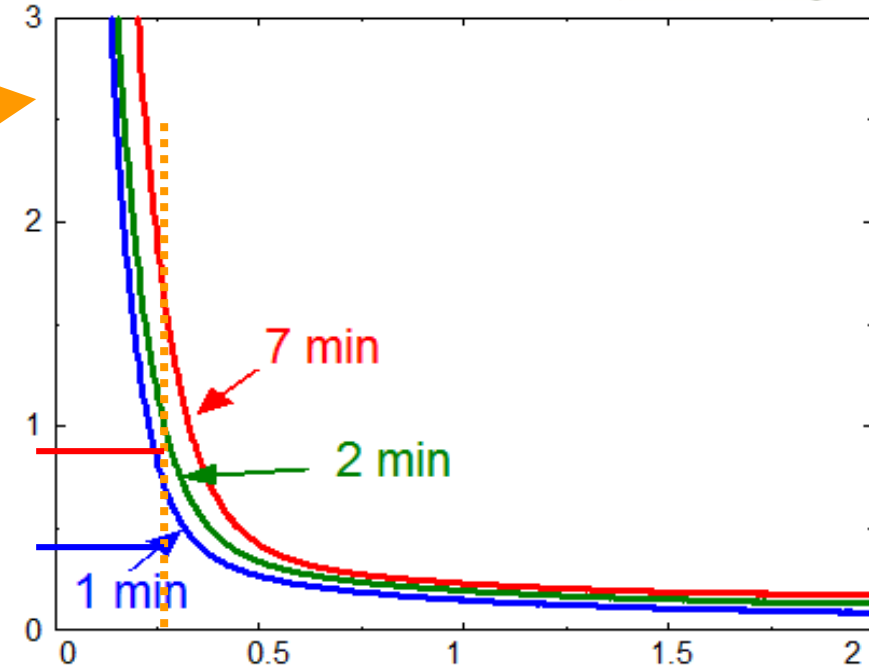
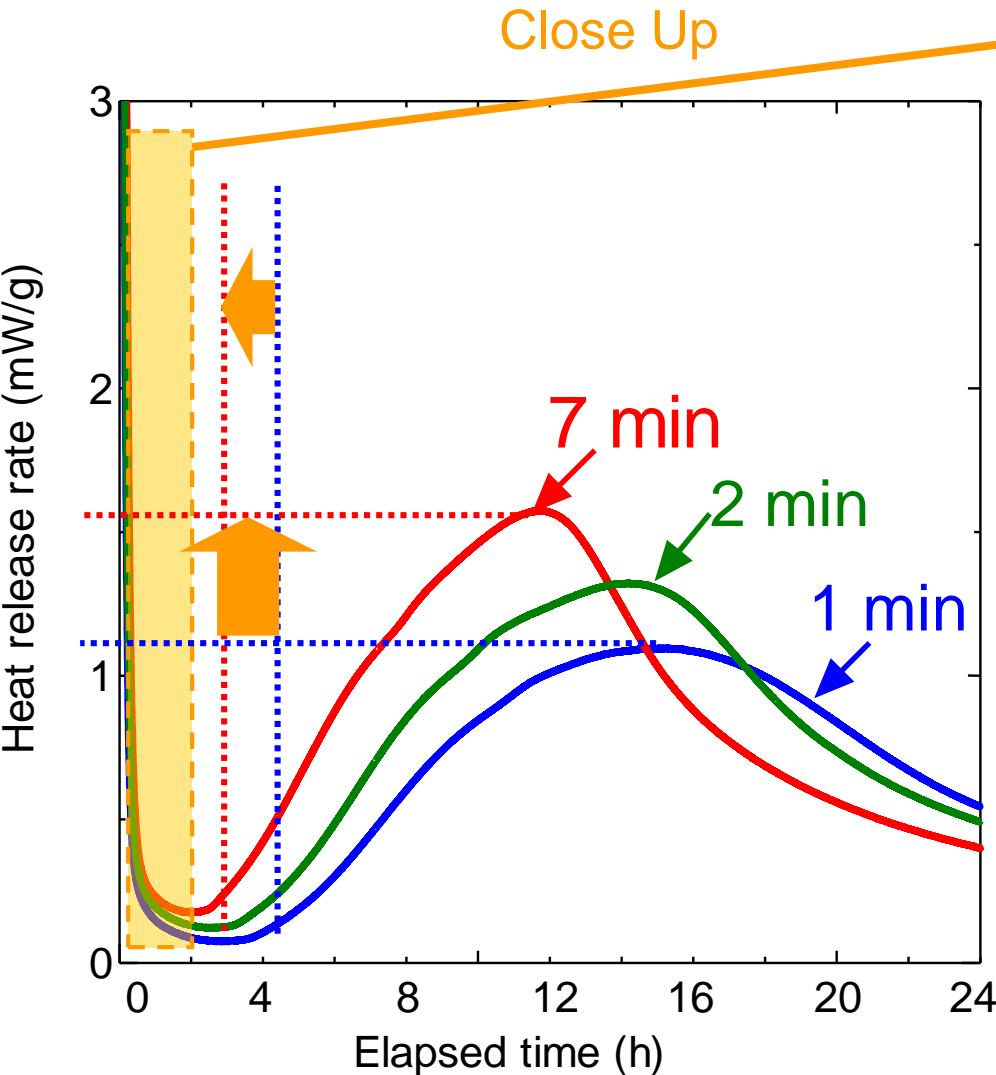
# The early hydration process



- Accelerated period (hardening process)
  - Metastable layer continuously dissolves
  - Ca<sup>2+</sup> & OH<sup>-</sup> increase slowly and approach the critical supersaturation of Ca(OH)<sub>2</sub>
  - Ca(OH)<sub>2</sub> and CSH grow at an exponential rate (massive hydration, 2<sup>nd</sup> peak)
- $$\text{C}_3\text{S}, \text{CSH(m)} + \text{H}_2\text{O} \rightarrow \text{CSH(s)} + \text{Ca(OH)}_2$$
- Set and increase in strength

Calorimetry curve for OPC paste

# Hydration and Calorimetry

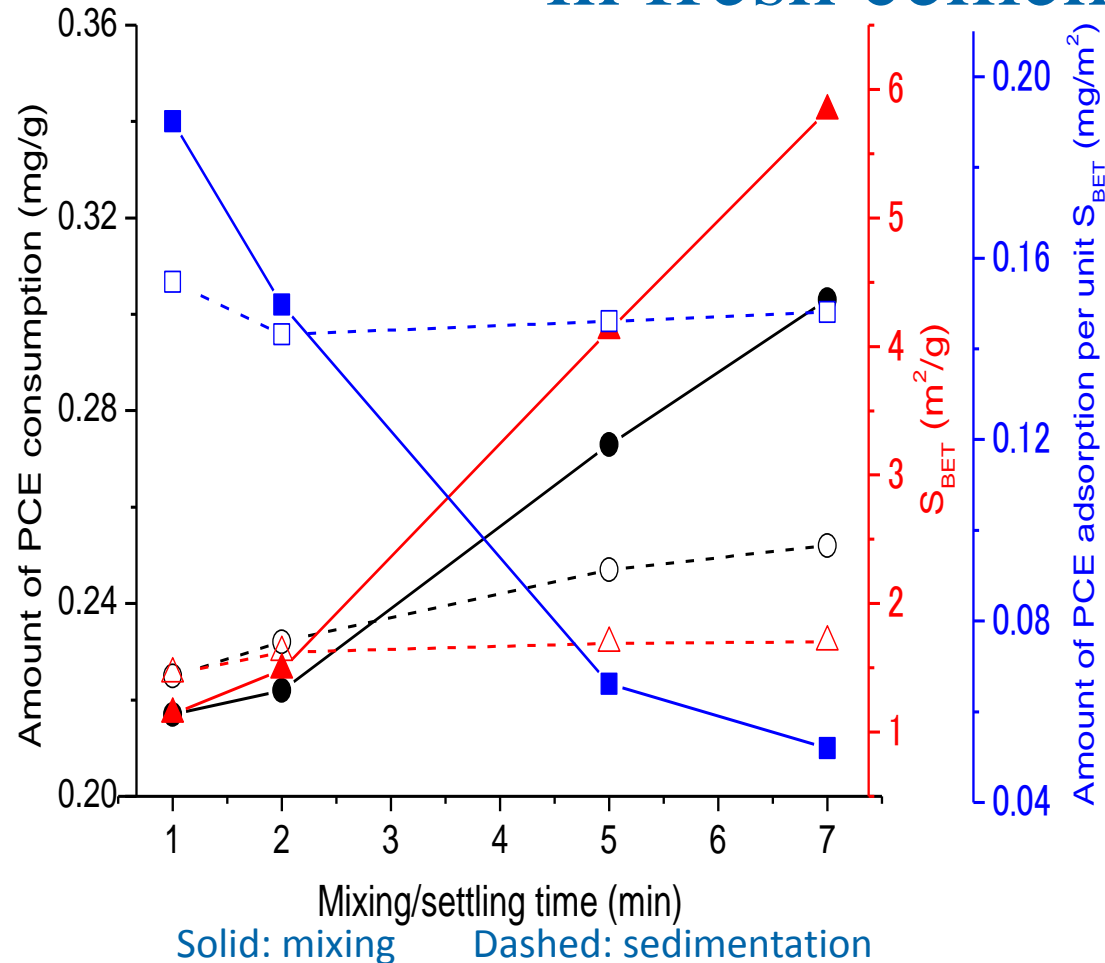


With increasing mixing time,

- Initial dissolution rate at a given time became more pronounced (**accelerated**)
- Start of massive hydration was advanced (**accelerated**)
- Second peak of the calorimetric curves increased



# Adsorption behavior of PCE in fresh cement paste



As mixing time became longer,

● Amount of PCE consumption in the solution phase increased

▲  $S_{BET}$  increased significantly

■ PCE adsorption per unit  $S_{BET}$  decreased

Sedimentation has little change

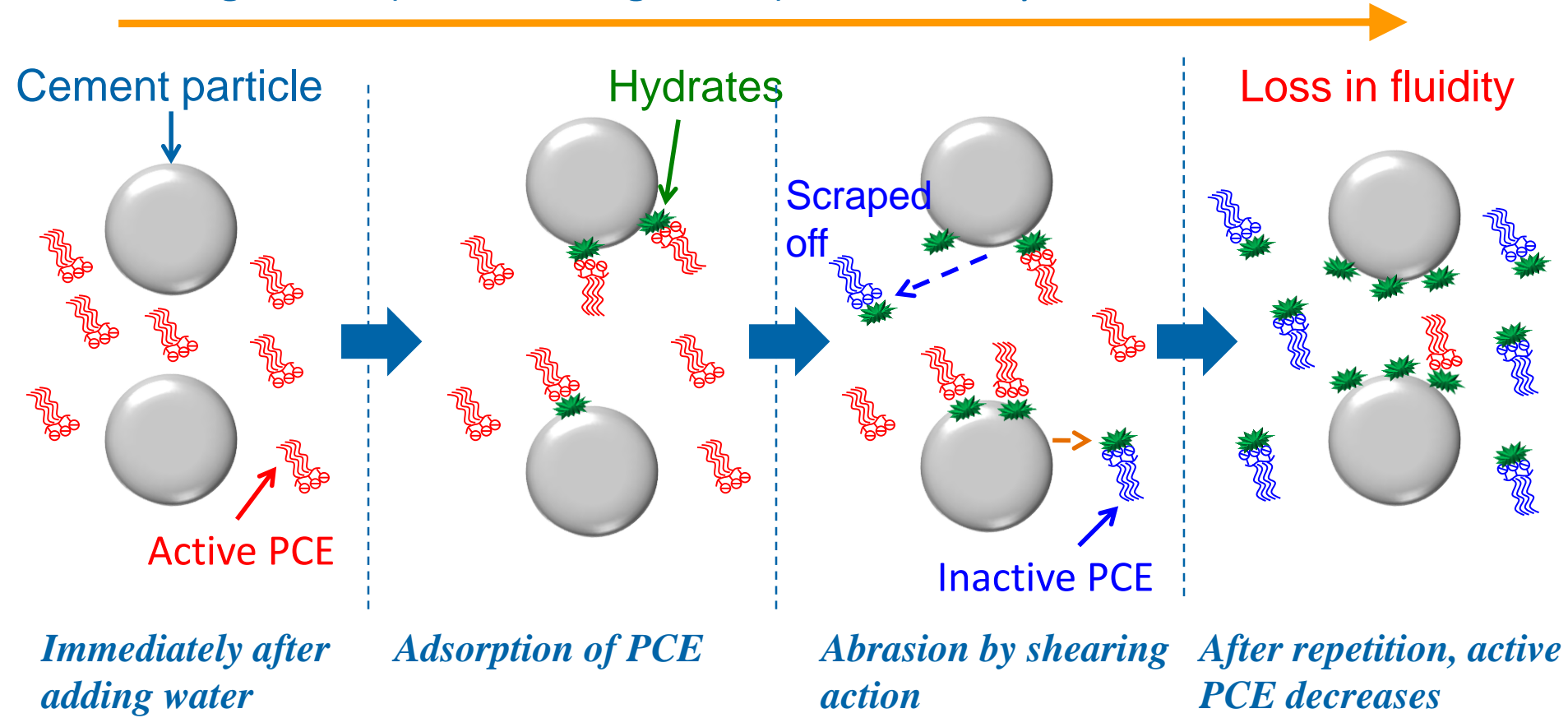
Extended surface area by mixing increases PCE consumption and subsequently causes degrading changes in fluidity

# Mechanism for changes in fluidity

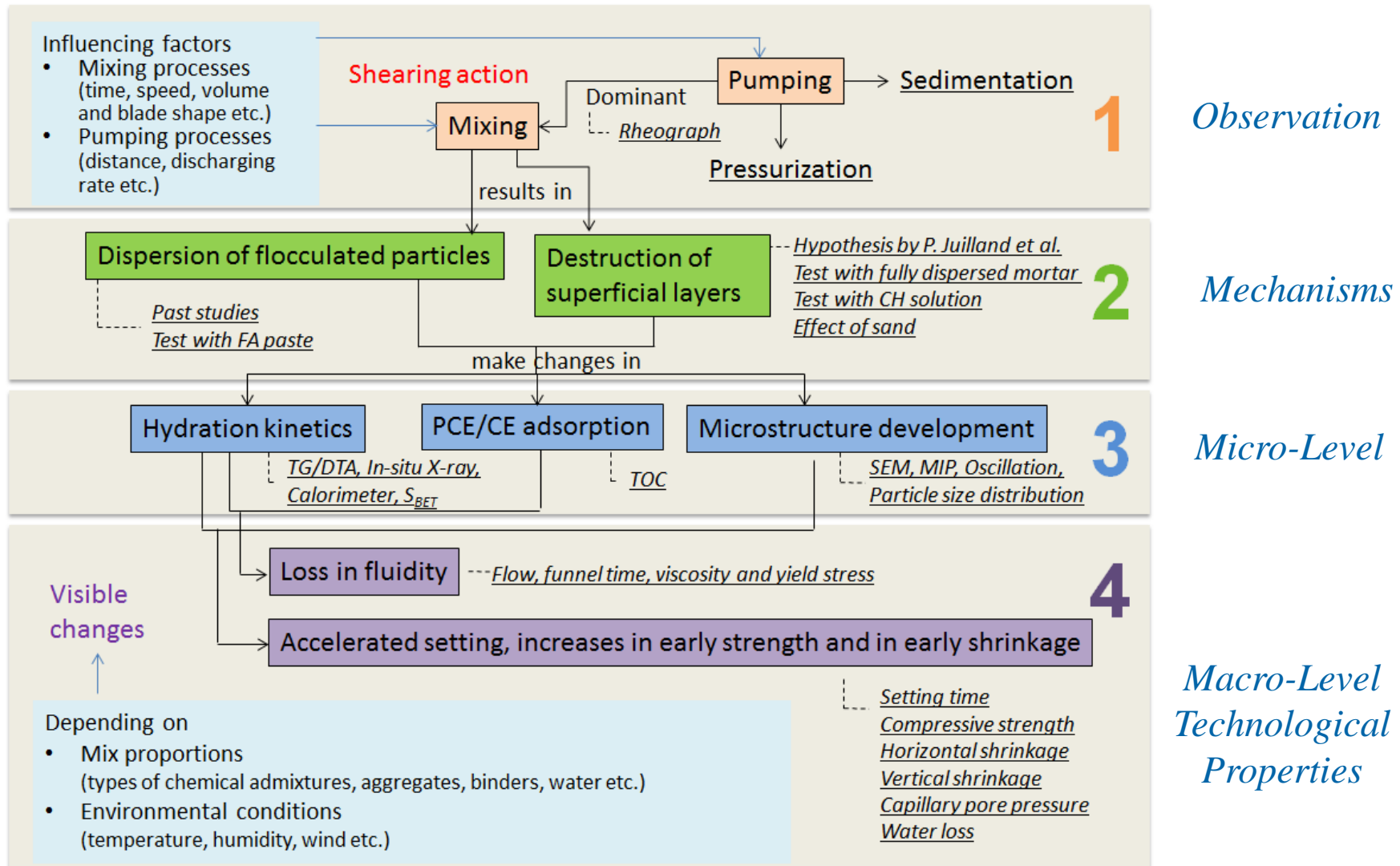


Active PCE adsorb onto hydrates and disperse cement particles

Shearing action (dominant factor) = Further hydrates formation



# Graphical Summary and Concept



# Conclusions

- ✓ With extended mixing or pumping distance
    - Yield stress and flow value decrease
    - Viscosity and efflux time increase
  - ✓ Analysis results using rheographs indicate
    - Shear stress during mixing and/or pumping is a major factor influencing mortar rheology
  - ✓ On a microstructural level
    - the consumption of active PCE in solution,
    - the increase in specific surface area of the cement
    - and a subsequent decrease for PCE per unit  $S_{\text{BET}}$
- can explain a change in state of dispersion and the observed changes in rheological properties

*Thank you for your  
attention!*