

Alkali-Activated and Geopolymer Cements: Design from Atoms to Applications

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Traditional and non-traditional cements



Most important: Designing materials that are fit for purpose!

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Adapted from: J.L. Provis & J.S.J. van Deventer (eds.), State of the Art Report of RILEM TC 224-AAM, 2014

Why alkali activation?

- Common SCMs are less reactive than clinker, reaction with water is slow
 - Chemical activation needed
- High-volume blended cements use PC clinker as activator – but it is not optimised for this task!
 - Clinker components & gypsum balanced to give optimal rheology, reaction & strength when used alone
 - If another material dominates, this is no longer optimal

→ Why not use a purpose-designed alkali activator instead?



e.g. Brisbane West Wellcamp Airport (Wagners; Australia)





http://www.engineersaustralia.org.au/portal/news/brisbane-west-wellcamp-airport-world%E2%80%99s-greenest

Some comments on "sustainability"

- Many studies calculate net CO₂ savings for alkaliactivated binders cf. Portland cement
 - Values range from 9 to 97% savings
 - Very few studies specific to an application or location, and few take care with reference concrete
- Realistic value probably ~40-80% in most locations and applications
- ~90% of environmental footprint of an alkaliactivated binder is from the activator (!)
 - Particularly if Na silicate is sourced from Na₂CO₃ produced using the Solvay process



How does it happen?





J.L. Provis & S.A. Bernal, Annual Review of Materials Research, 2014, 44: 299-327

Gel chemistry

- Alkali activation with low calcium N-A-S-(H) ('geopolymer') gel
 - Fly ash, metakaolin precursors
 - Pseudo-zeolitic structure, sometimes minor crystalline inclusions
 - Little chemically bound water



- Alkali activation with more calcium C-A-S-H type gel
 - Low C/S ratio, high Al content, generally more cross-linked than PC hydration products
 - Secondary phases mostly layered double hydroxides (hydrotalcite/AFm)
 - Some bound water (space-filling)





J.L. Provis & S.A. Bernal, Annual Review of Materials Research, 2014, 44: 299-327

Differences in space-filling character





Data from X-ray µCT (APS 2-BM-B): J.L. Provis et al., Cem. Concr. Res., 2012, 42(6):855-864.

NordTest chloride migration – low penetration











(all concretes of comparable 56-day strength, & similar total pore volume according to ASTM C642)



I. Ismail et al. Constr Build Mater 48 (2013):1187-1201.

- Can C-A-S-H and N-A-S-H gels really coexist in a stable state?
- What happens to the water in the gel, and can we control this?
 - \rightarrow How does this influence properties in service?

Best available approach: Linking experimental characterisation with thermodynamic modelling

(...only for C-A-S-H so far, no model for N-A-S-H yet)



Thermodynamic modelling



$$G_{m} = \left[\sum_{n_{1}}\sum_{n_{2}}\sum_{n_{3}}\cdots\sum_{n_{s}}\left(y_{i_{1}}^{n_{1}}y_{i_{2}}^{n_{2}}y_{i_{3}}^{n_{3}}\cdots y_{i_{s}}^{n_{s}}\right)\cdot^{o}G_{i_{1}i_{2}i_{3}}\cdots i_{s}\right] + R^{*}T\left[I\sum_{i_{1}}\left(y_{i_{1}}\ln\left(y_{i_{1}}\right)\right) + II\sum_{i_{2}}\left(y_{i_{2}}\ln\left(y_{i_{2}}\right)\right) + III\sum_{i_{3}}\left(y_{i_{3}}\ln\left(y_{i_{3}}\right)\right) + \cdots + \zeta\sum_{i_{s}}\left(y_{i_{s}}\ln\left(y_{i_{s}}\right)\right)\right] + G_{m}^{E}$$

 $(CaO)_{a'}(SiO_{2})_{b'}(Al_{2}O_{3})_{c'}(Na_{2}O)_{d'}(H_{2}O)_{e'(s)} \xrightarrow{K_{so}} a'Ca^{2+}_{(aq)}$ $+ b'SiO_{3}^{2-}_{(aq)} + 2c'AlO_{2}^{-}_{(aq)} + 2d'Na^{+}_{(aq)} + 2(a'-b'-c'+d')OH^{-}_{(aq)}$ $+ (b'+c'+e'-a'-d')H_{2}O_{(l)}$



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R.J. Myers et al. Cement & Concrete Research 66(2014):27-47

Phase and volume stability



CNASH_ss model has a more dense C-(N-)A-S-H gel than previous work just based on C-S-H



R.J. Myers et al. *Applied Geochemistry*, 61: 233-247

Validation of CNASH_ss: AAS (C-M-N-K-S-A-S-H) system

AAS pore solution chemistry described accurately



Literature data for pore solutions extracted from cements made of BFS with $NaOH \cdot mH_2O$ or $Na_2O \cdot rSiO_2 \cdot mH_2O$; reaction extents estimated where needed



R.J. Myers et al., Cement and Concrete Research, 2014, 66, 27-47.



Controlling shrinkage?

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Blast furnace slag + Na₂SiO₃ activator





Slag chemistry and durability



→ Slag chemistry plays an important role in determining the performance of alkali-activated slag binders



S.A. Bernal et al., Cement & Concrete Research, 57(2014):33-43

Can we predict this?

Blast furnace slag + Na₂SiO₃ activator



Important differences depending on Mg-Al LDH phase...



R.J. Myers et al. Applied Geochemistry, 61: 233-247

Accelerating carbonate activation

Adding calcined layered double hydroxide (CLDH) (hydrotalcite, 500°C)



- In an Na₂CO₃-activated binder system, slags containing higher levels of MgO react much more rapidly
- Incorporation of 10 wt.% CLDH in sodium carbonate activated slag pastes accelerates the reaction, enabling setting within 24 hours.



X. Ke et al. 2016. Cement and Concrete Research, 81, 24-37.

How does CLDH work?

In a slag-based binder activated by Na₂CO₃:

- Accelerated consumption of carbonate ions
- Increasing the pH of the activator
- Hydrotalcite nucleation seeding





X. Ke et al. 2016. Cement and Concrete Research, 81, 24-37.

Increasing chloride binding

Before and after chloride exposure (slag M06), data from SEM-EDX



- Close correlation between Cl/Si ratio and Mg/Si ratio
- Higher Mg/Si ratio is related to LDH regions, these selectively bind Cl⁻
- Mg/Al ratio of LDH phase is ~1.6

Iniversity

X. Ke. PhD (Sheffield), in progress.

So – what is really needed?

- Most important the right application (!)
- Material (and application) must be 'sustainable'
 - Financially and environmentally
 - Reliable and sufficient volume supply of raw materials? Activator?
 - Mix design must be efficient admixtures??
- Material must be durable
 - Replacement/repair is expensive design for durability at both cement and concrete levels, including creep (?)
- Material must be robust



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