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AUCKLAND
Te Whare Wānanga o Tāmaki Makaurau
NEW ZEALAND

Residual Capacity of Damaged and Epoxy-Repaired Reinforced Concrete Plastic Hinges

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Objective and scope



Key questions:

- What are the implications of the observable damage?
- What is the capacity in the damaged state?
- What is the capacity after epoxy repair?

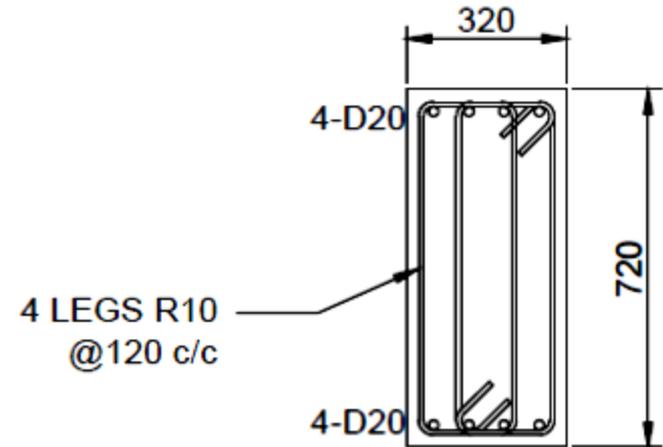
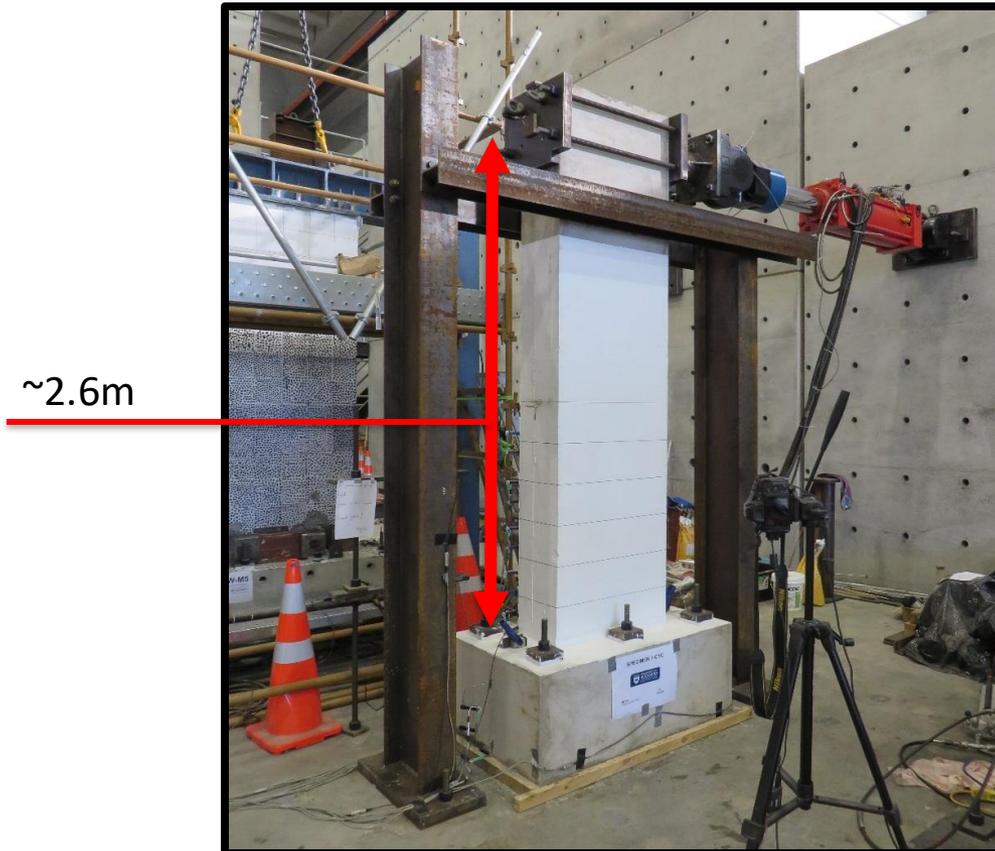
Focus is on 'moderate' plastic hinging damage:

- No crushing of core concrete
- No buckled or fractured reinforcement
- No wide shear cracks indicating yielded transverse reinforcement



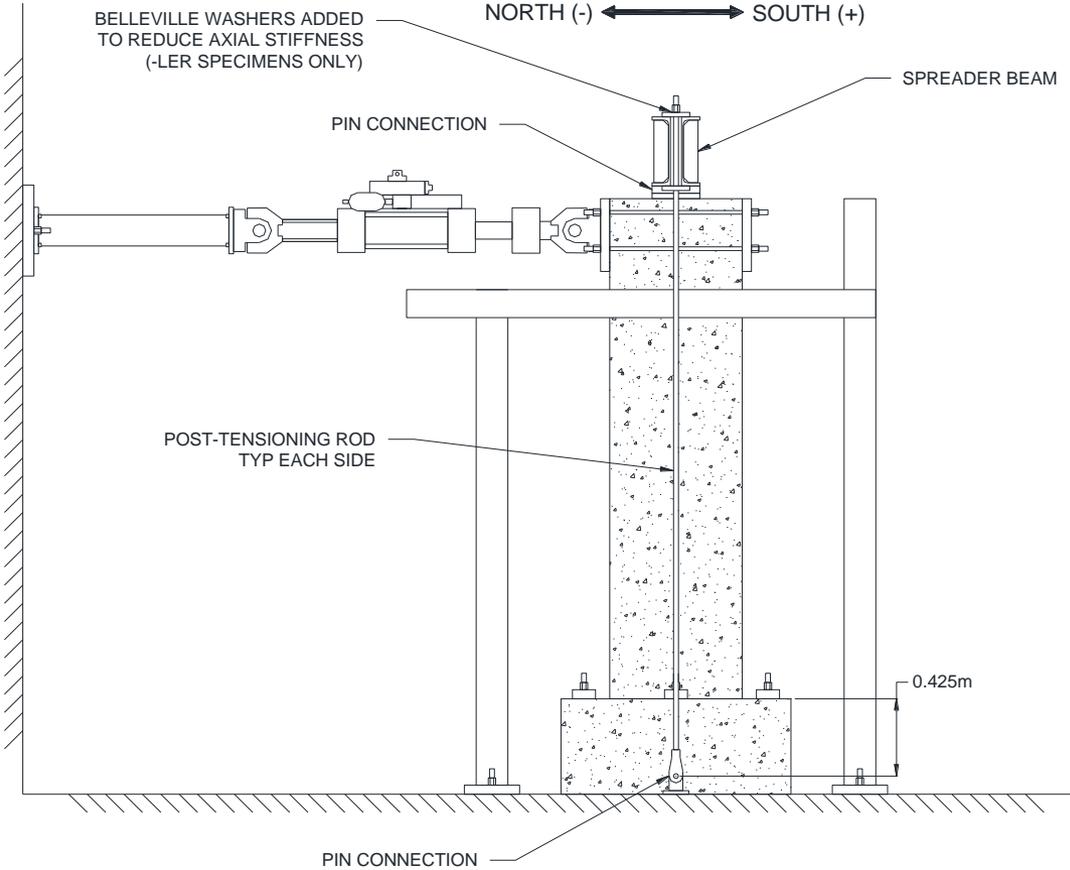
Focus is on beams, but the research has implications for columns and walls

Test program (17 identical beam specimens)



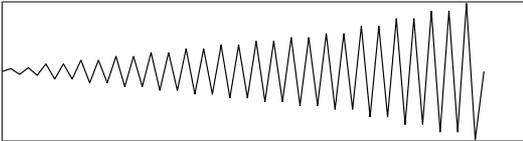
Complies with ACI 318 SMRF and
NZS 3101:2006 'ductile' beam

Axial restraint system

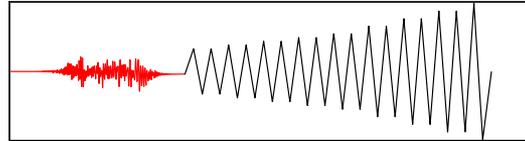


Loading protocols

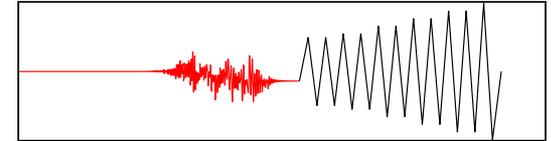
Type CYC



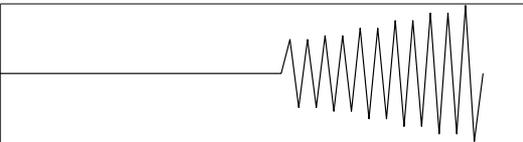
Type LD-1



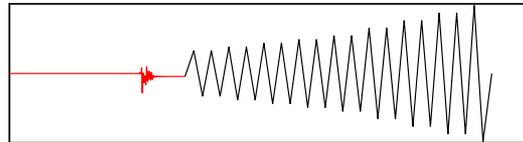
Type LD-2



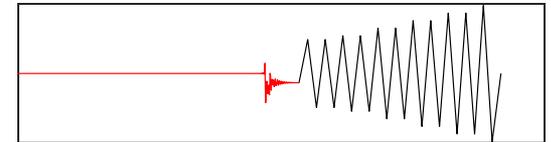
Type CYC-NOEQ



Type P-1



Type P-2



1.4% peak drift during
earthquake

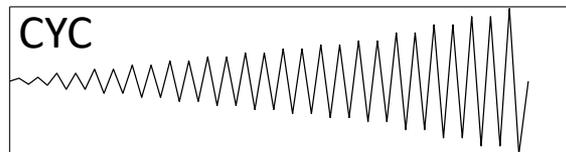
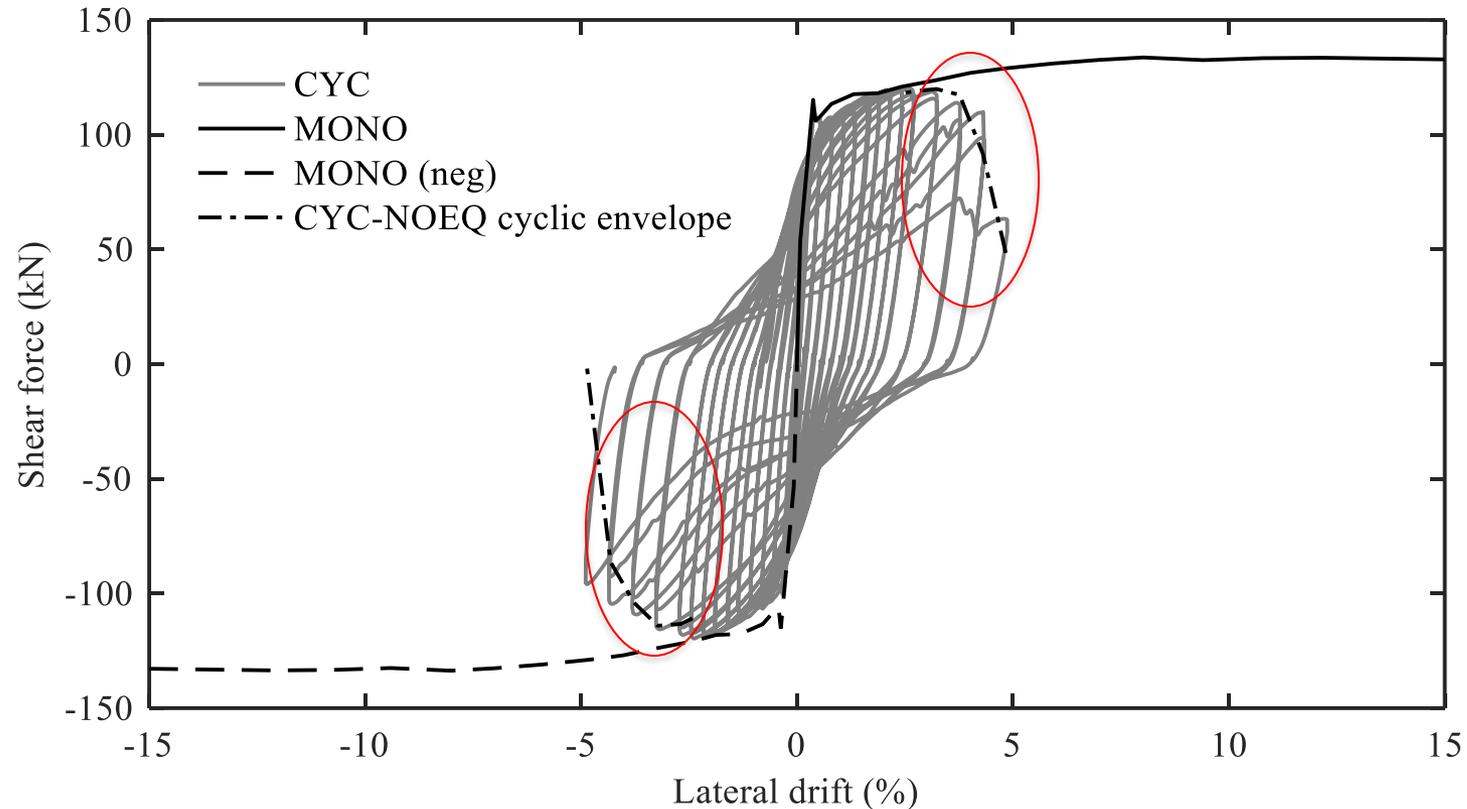
2.2% peak drift during
earthquake

Red = Earthquake-type displacement history

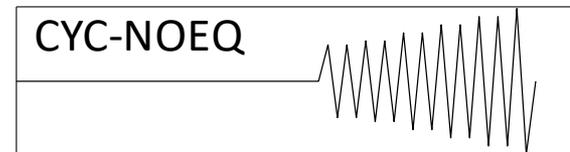
LD = Earthquake displacement history derived using a **long duration** ground motion

P = Earthquake displacement history derived using a **pulse-type** ground motion

Effect of moderate-level loading cycles

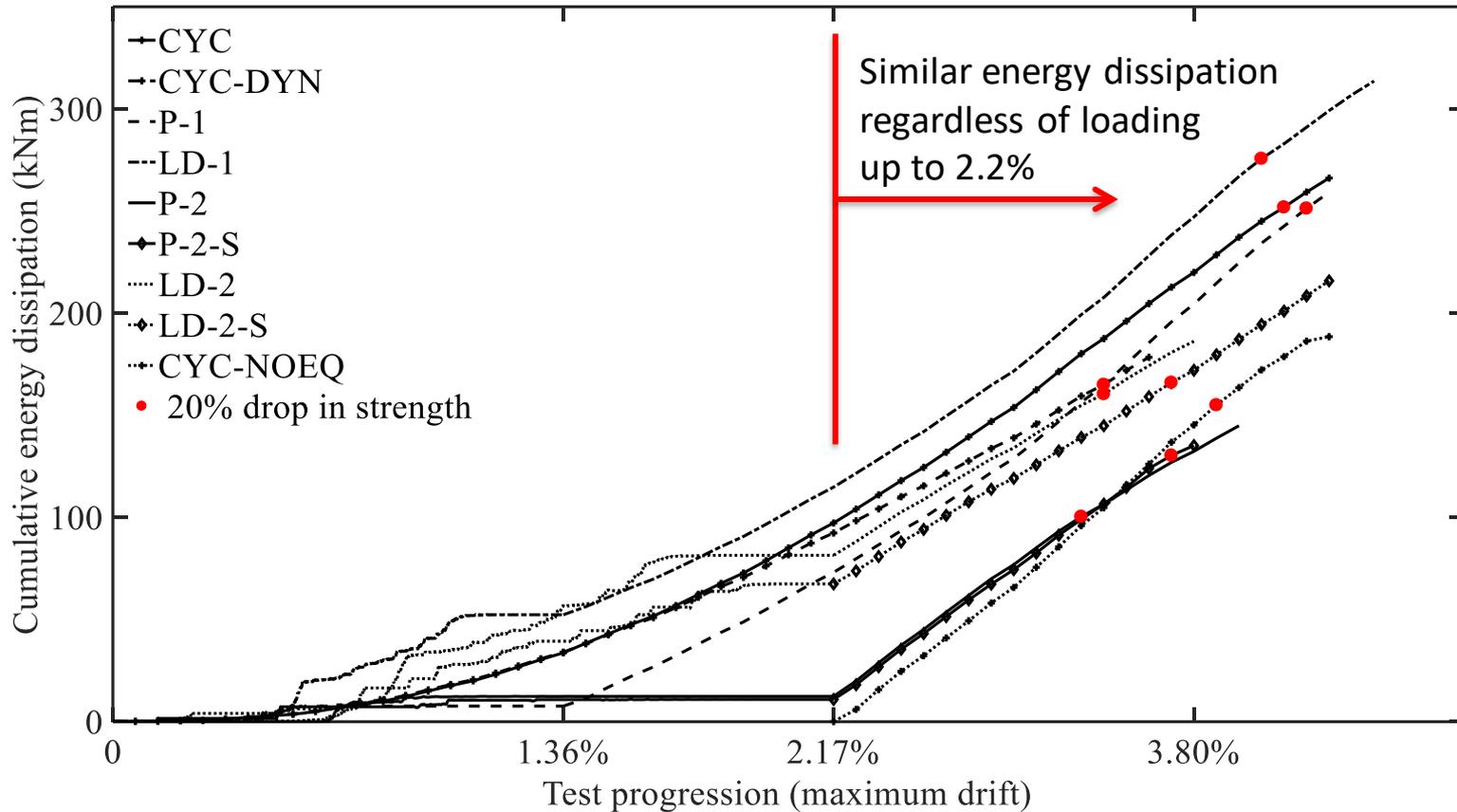


VS



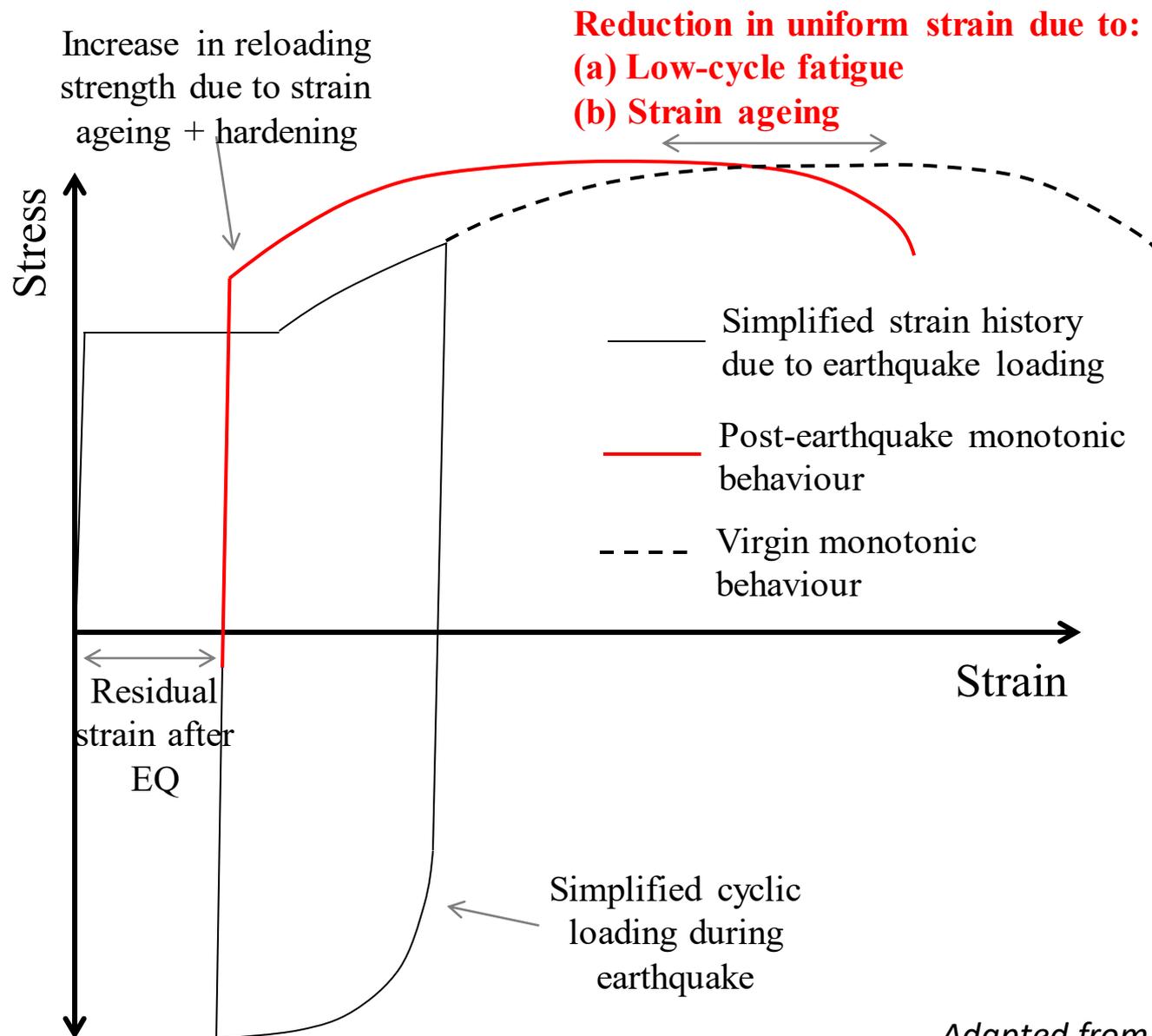
No change in deformation capacity!

Effect of moderate-level loading cycles

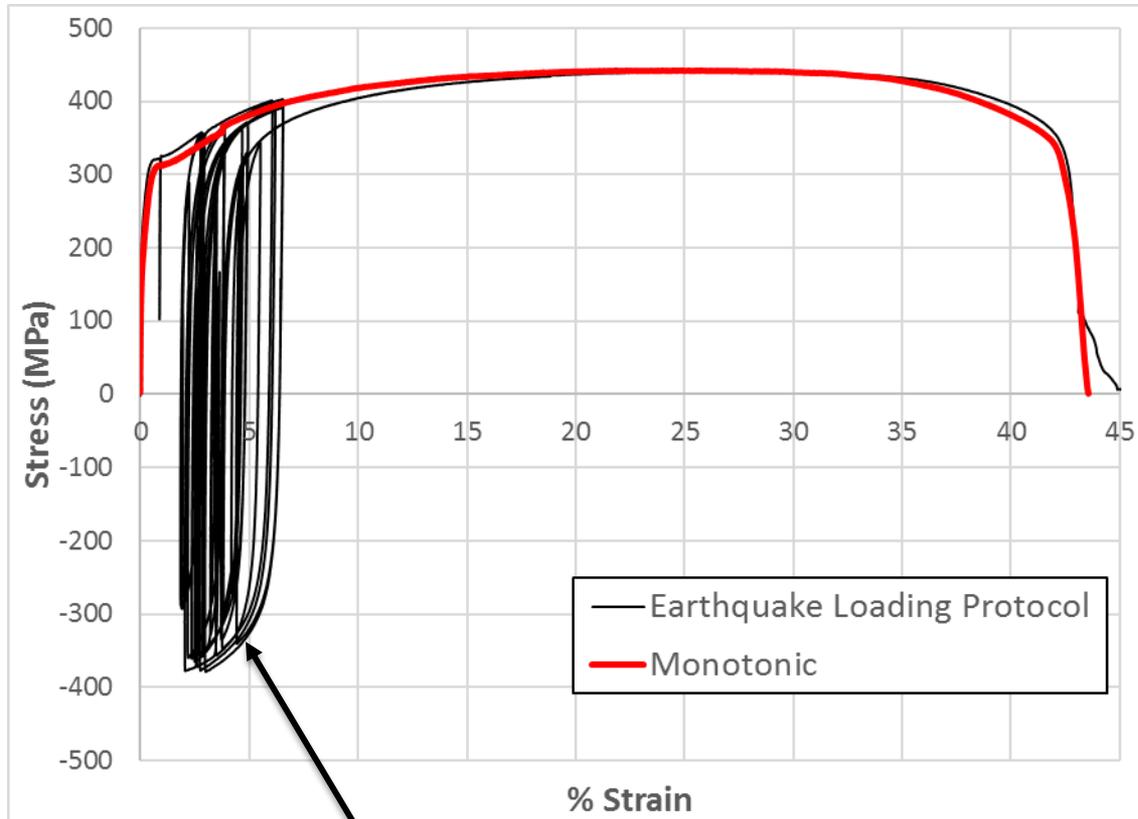


Variation in energy dissipation due to the different loading protocols carried through until failure.

Reduction in steel strain capacity



Reduction in steel strain capacity -Low-cycle fatigue

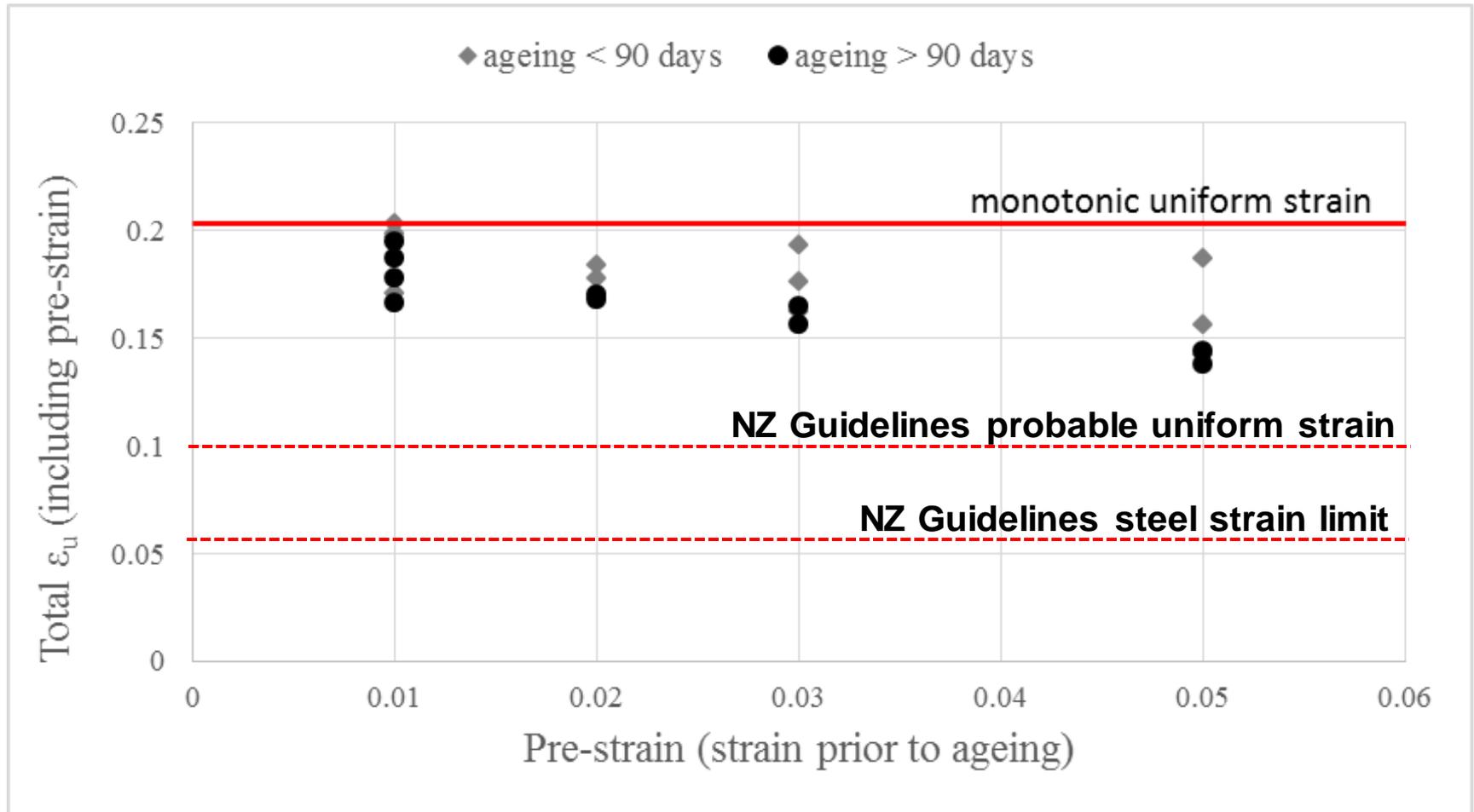


Strain demands from bar from long-duration beam test scaled to 6% max strain



Marder (2018)

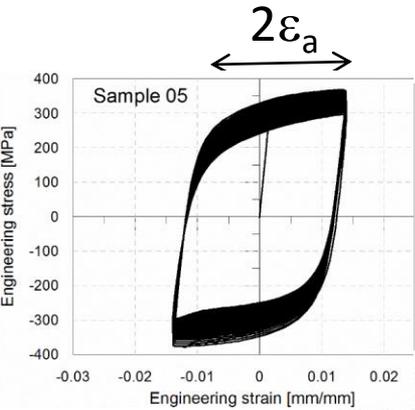
Reduction in steel strain capacity - Strain ageing



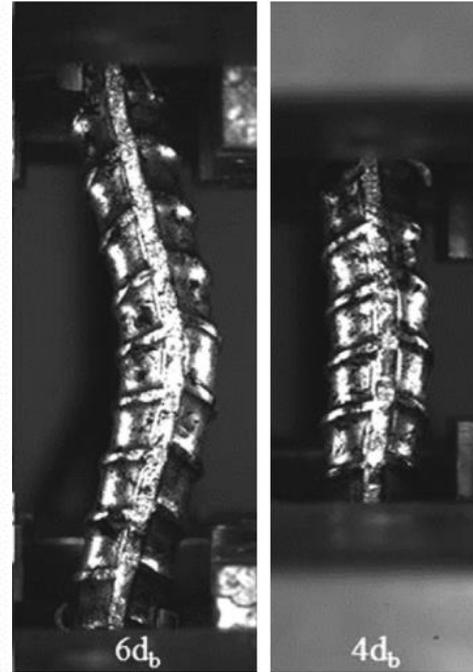
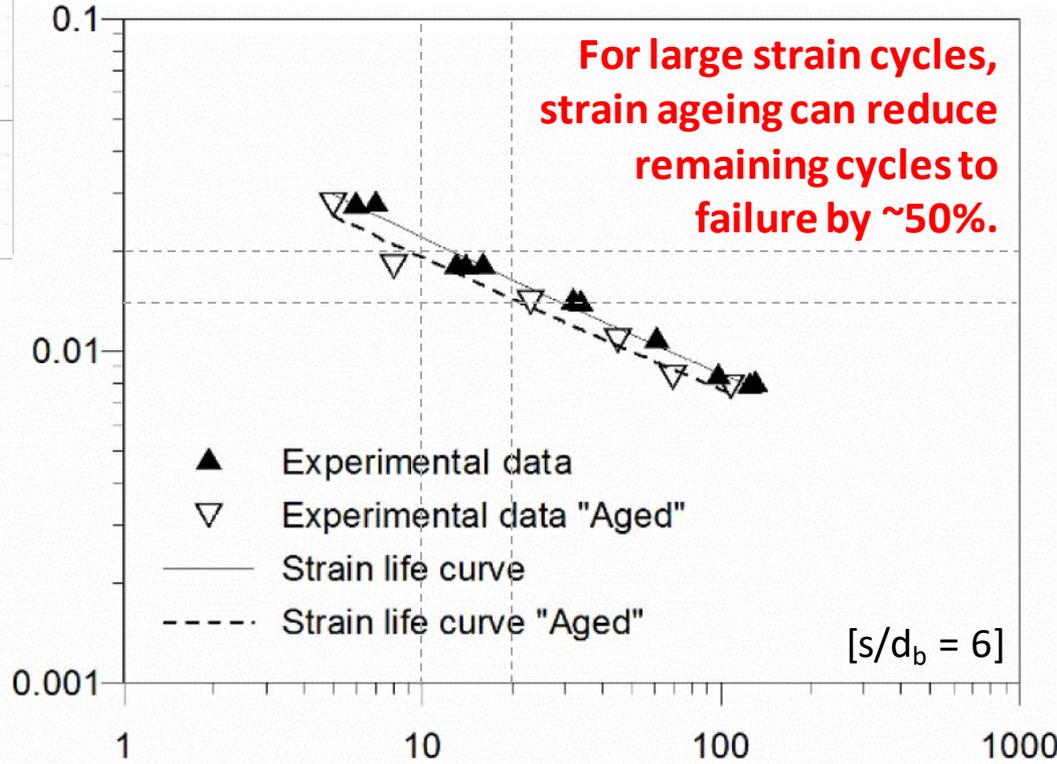
Data: Restrepo-Posada et al (1994) and Loporcaro et al (2016)

Reduction in steel strain capacity

- Strain ageing + LCF



Loporcaro (2017)

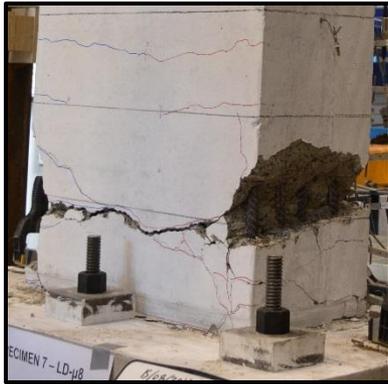


Ghannoum and Slavin (2016)

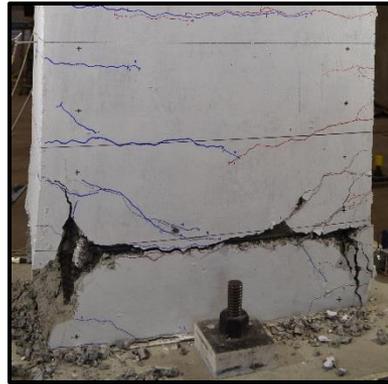
Typ. pulse GM

Typ. subduction or other long duration GM??

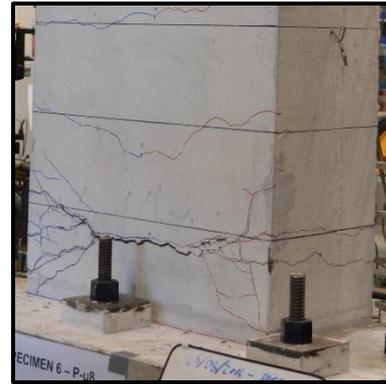
So does moderate damage 'reduce' the residual capacity?



LD-2



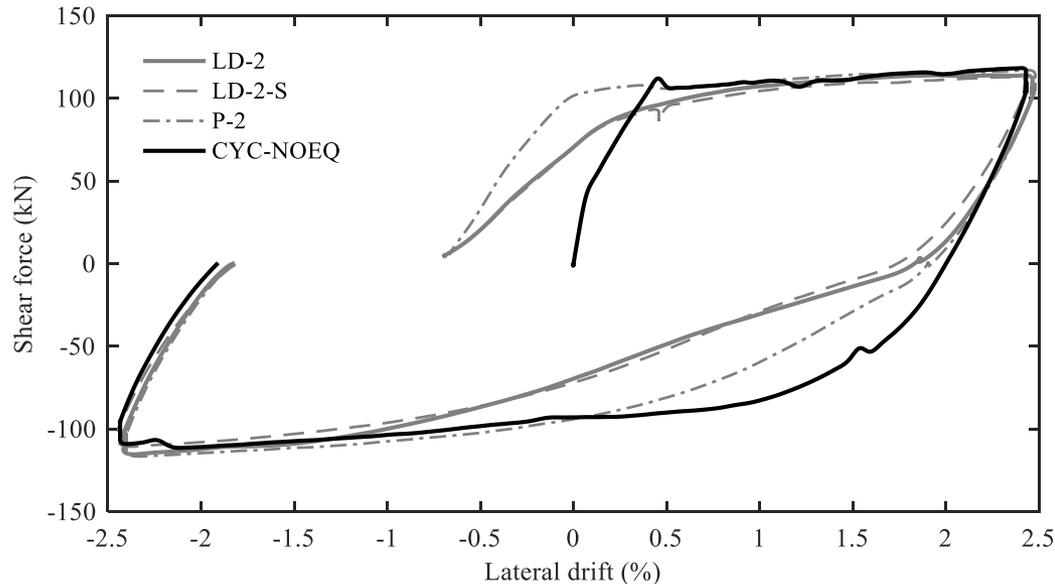
LD-2-S



P-2

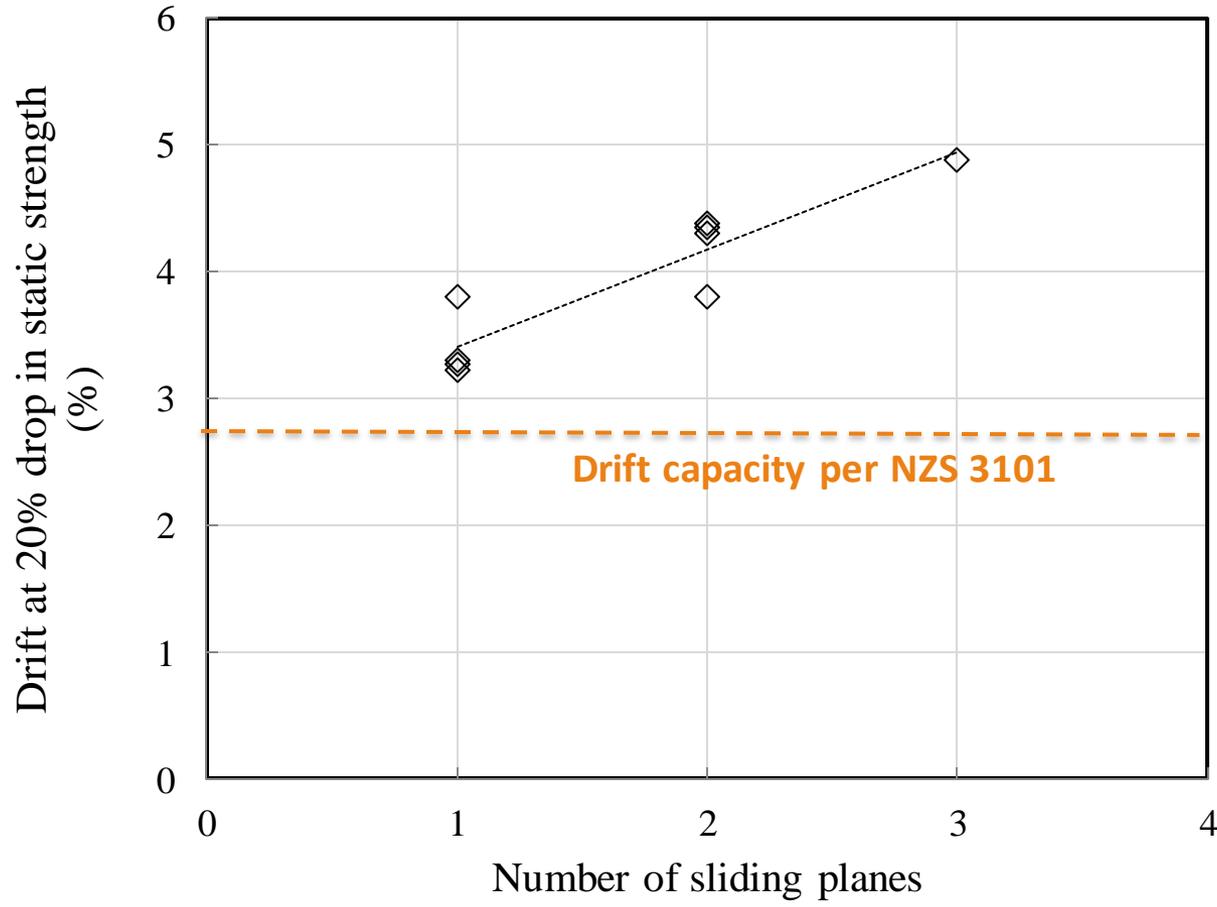


CYC-NOEQ



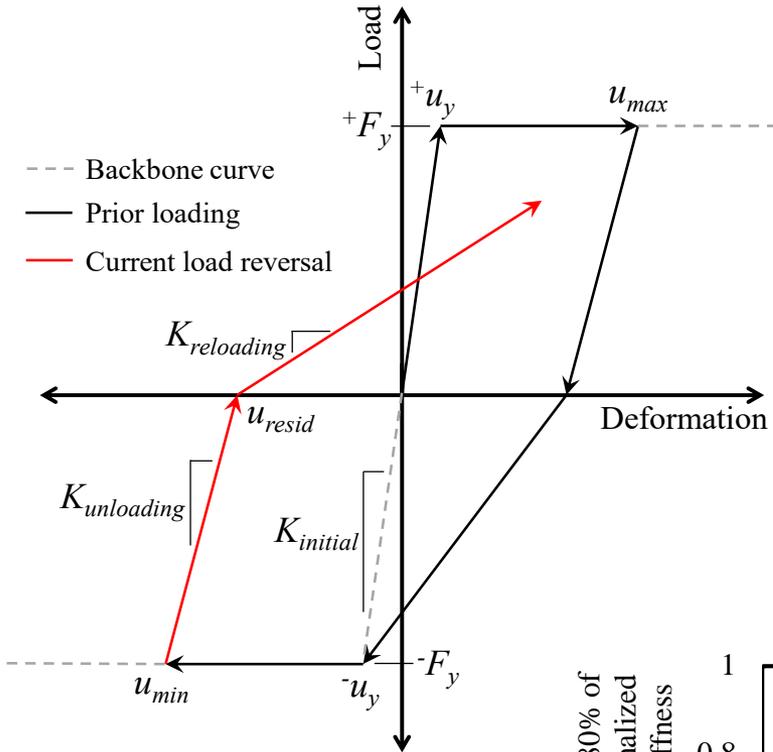
- Stiffness is reduced
- Strength is not reduced
- Deformation capacity is not 'reduced' – but post-earthquake assessments may provide insight for improved assessment of deformation capacity

Damage → Drift capacity?



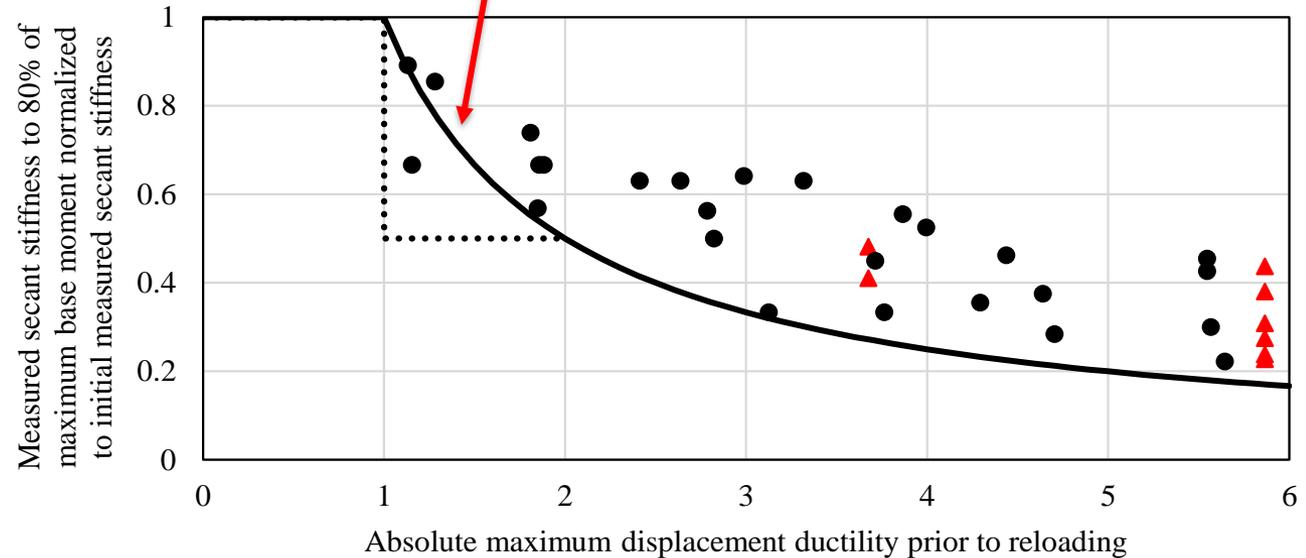
→ *Drift capacity correlated with number of sliding planes.*

How much stiffness is lost?



$$\frac{K_r}{K_y} = \frac{1}{\mu}$$

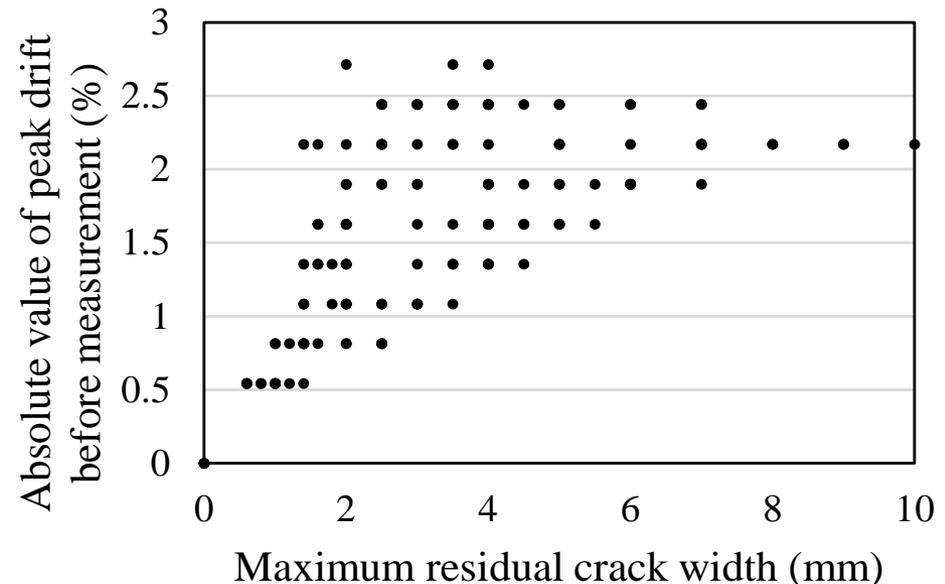
- Circular columns - after previous shake table tests
- ▲ Beam specimens - after initial earthquake loadings



How to estimate the peak deformation demands during the damaging earthquake?

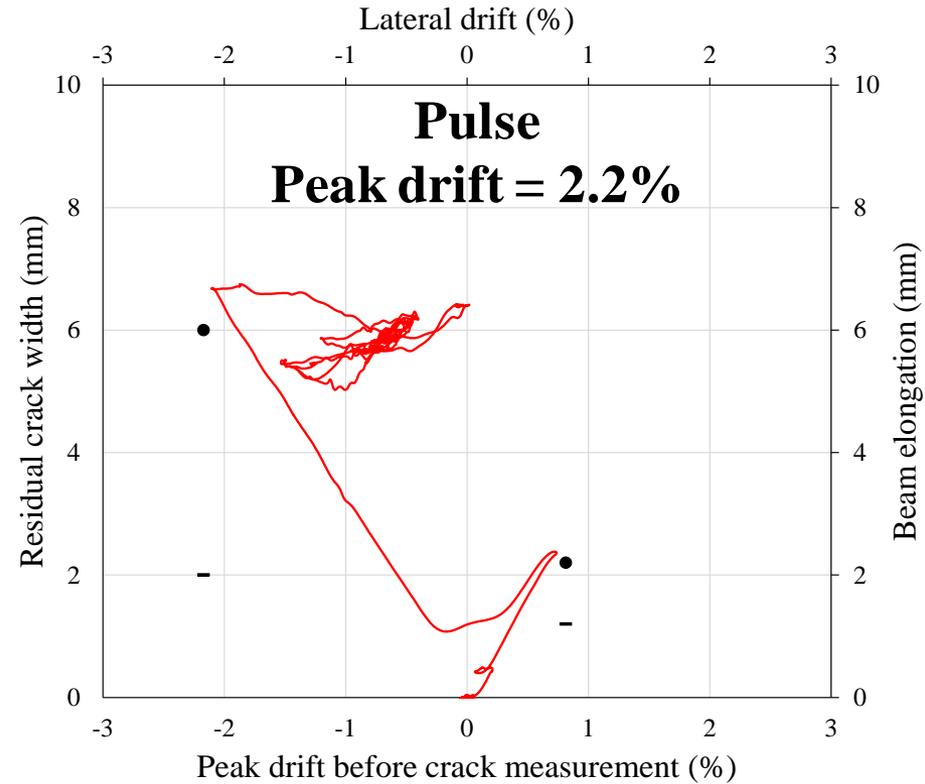
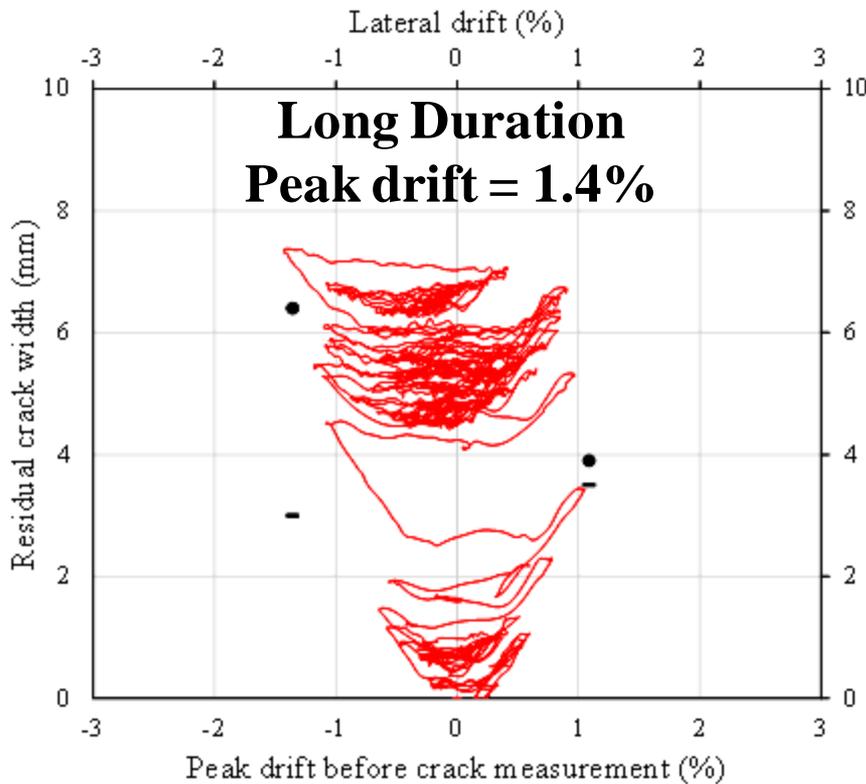
- Very important to understand the demands imposed on a damaged building before trying to assess it.
- No sense conducting a detailed seismic assessment on a damaged building if you can't evaluate how it responded in the first earthquake!

Existing post-earthquake assessment guidelines use the maximum residual crack width as a key damage indicator



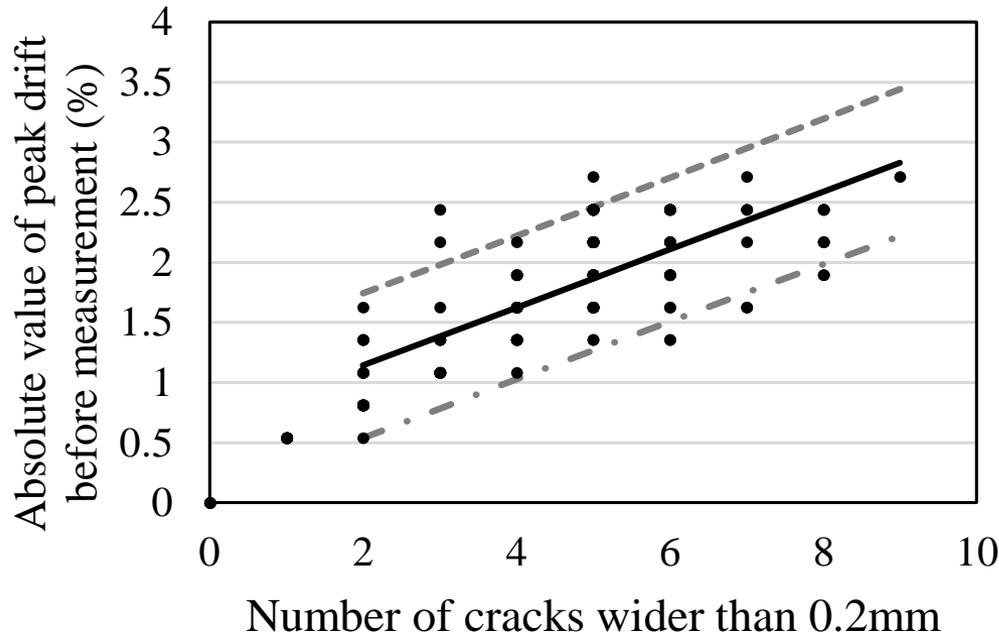
Residual crack widths versus elongation

● Total crack width - Maximum crack width — Elongation



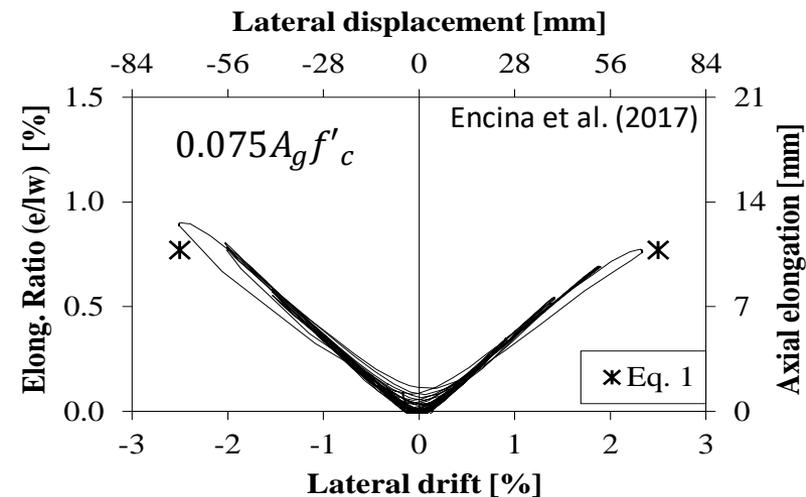
Similar residual
crack widths!

Distribution of cracking metrics?

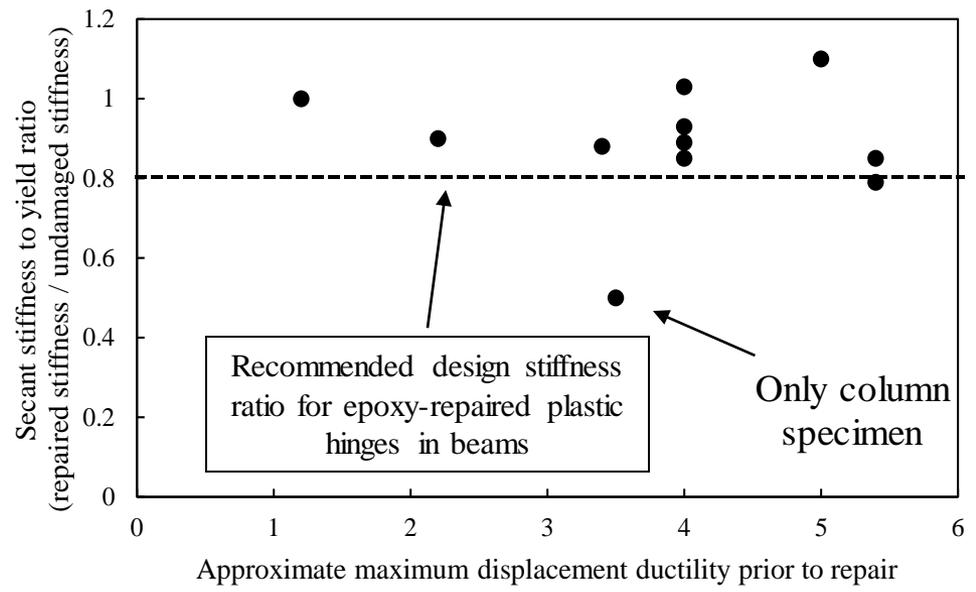
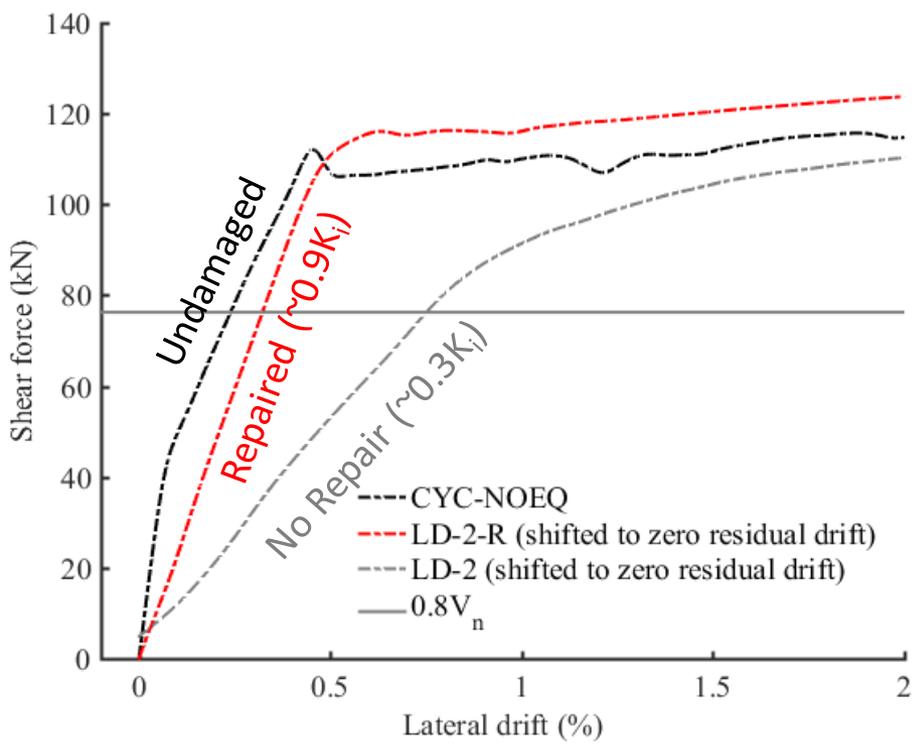
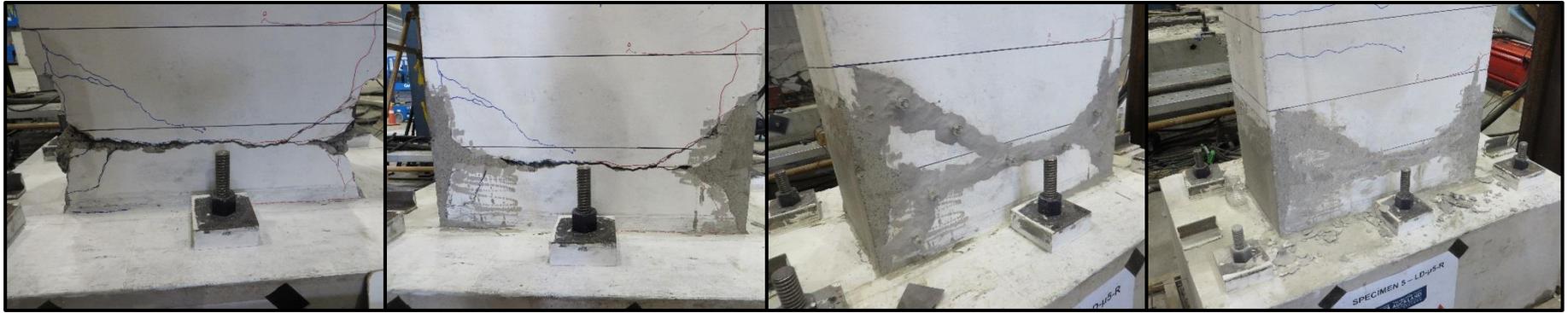


Single crack in beams (with min. reo) is an indicator of low rotation demands

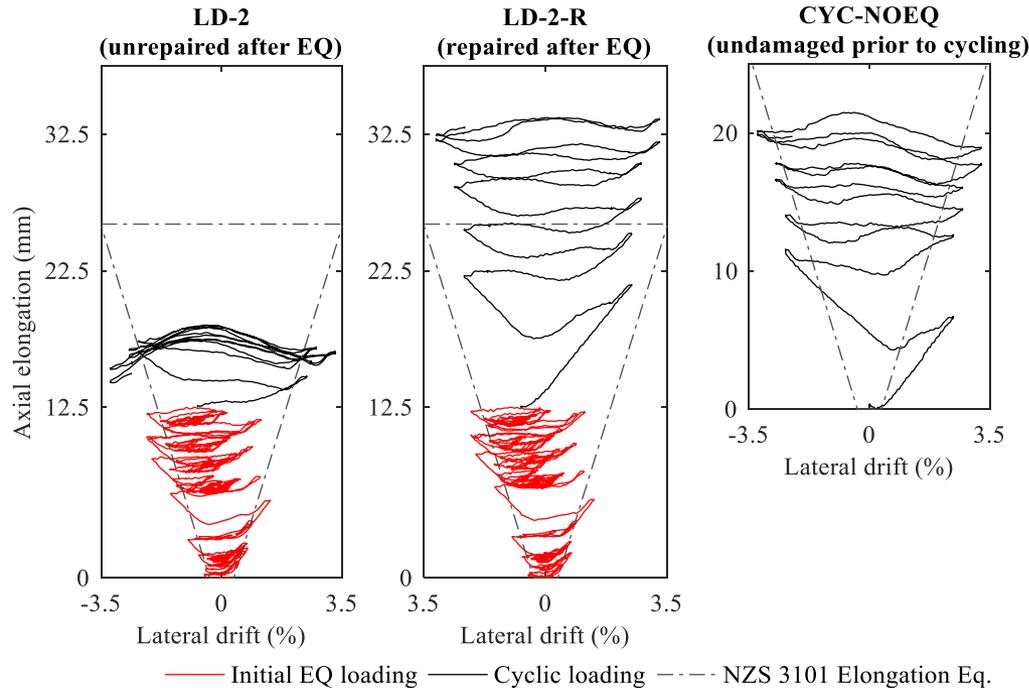
Columns & Walls?



Epoxy repair

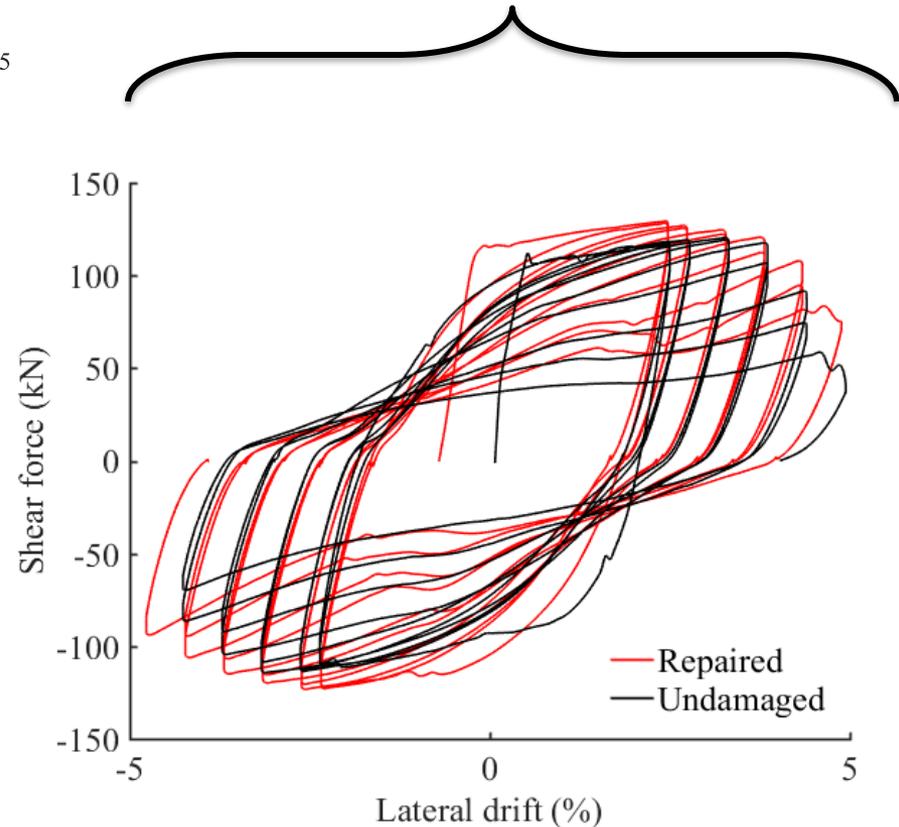


Epoxy repair



- Post-repair **strength increases** as a result of higher reo strain.
- **Deformation capacity** is similar between repaired and undamaged cases

Residual elongation at the time of repair causes an **increase in cumulative elongation** (and therefore longitudinal reo strain!)



Repair after failure – strain aged bars



New bars welded in on side
with buckled bars



Old concrete hydro-demolished

New concrete poured



Damage after original test:
Bars only buckled on one
side. Approx. 25mm
residual elongation.

Unbuckled bars left in place

Repair after failure – strain aged bars

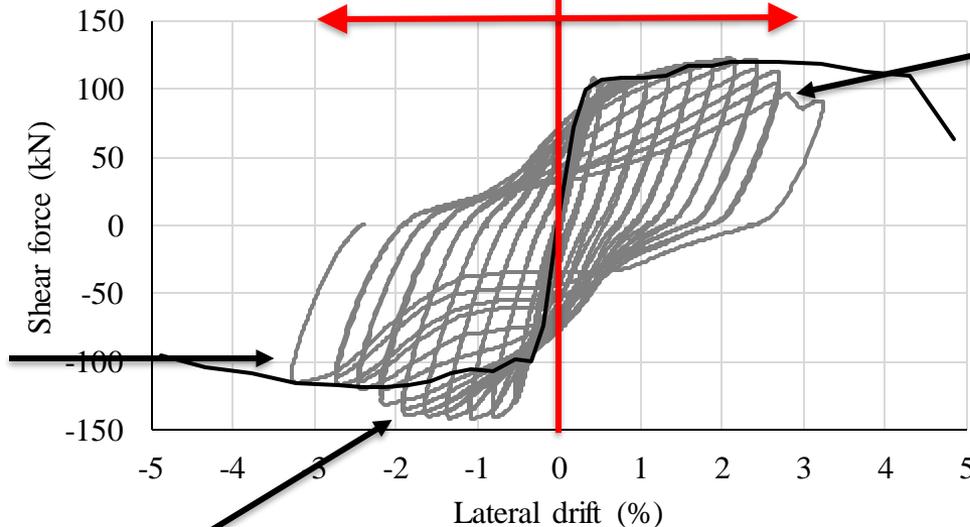
Testing six months after original test. Strain aged bars again didn't buckle



Prior strained bars in tension

Repaired bars in tension

Early failure in new bars due to strain concentration between welds



No fracture of strain aged bars

Strength increase due to strain ageing

Summary



- Prior loading cycles below 2% drift have minimal impact on drift or energy dissipation capacity.
- Residual crack widths alone do not provide reliable estimate of peak drift demands.
- Prior earthquake loading results in reduction in stiffness proportional with ductility demand.
 - Epoxy repair can recover 80% of original stiffness



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Thank you

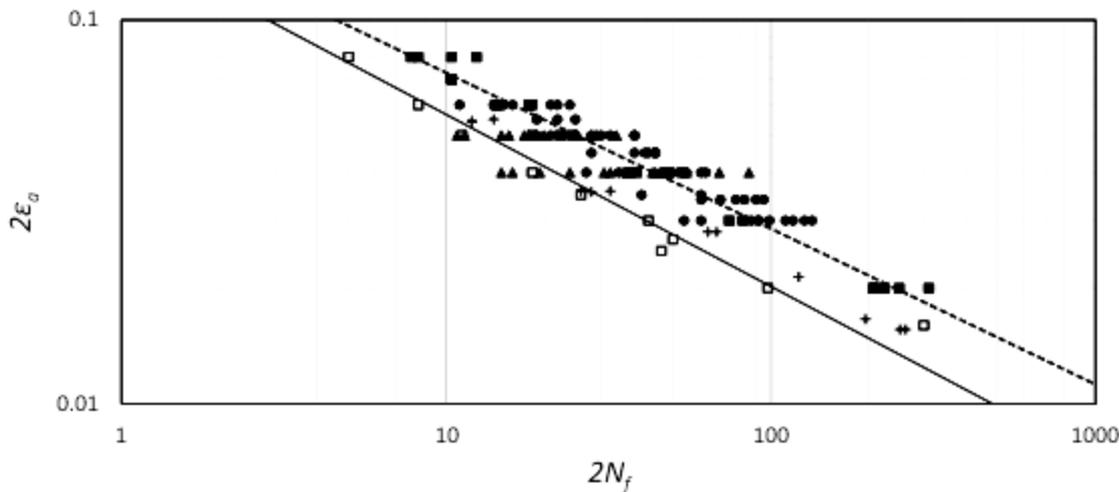


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What about low-cycle fatigue?

Coffin-Manson equation: $\epsilon_a = \epsilon'_f (2N_f)^c$

- Mander et al. (1994)
- ▲ Ghannoum and Slavin (2016)
- Brown and Kunath (2004)
- Hawileh et al. (2010b)
- + Loporcaro (2017)
- Coffin-Manson equation (Mander et al. data)
- - - Coffin-Manson equation (All data with clear spacing 4d_b or less)



For unbuckled bars: $\epsilon_a = 0.093(2N_f)^{-0.41}$

Equivalent to 40 cycles at a strain reversal of 0.03

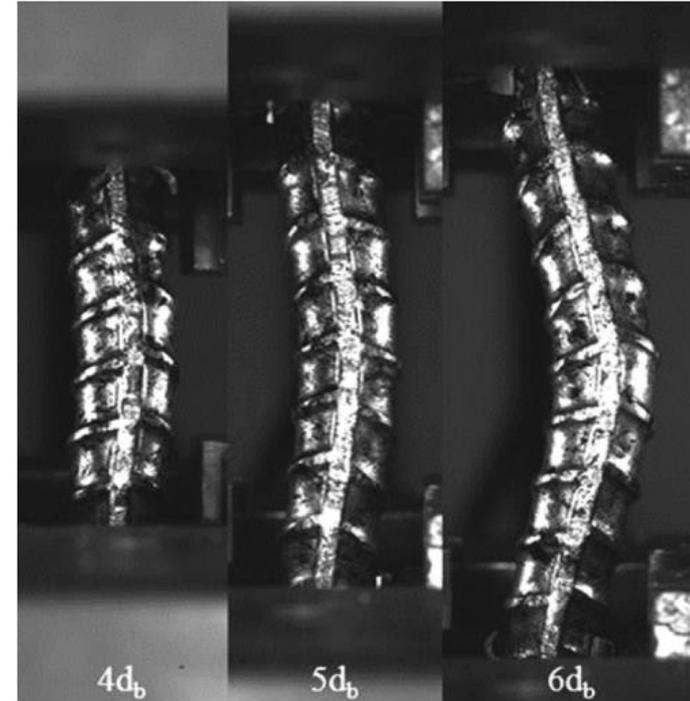
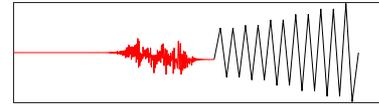


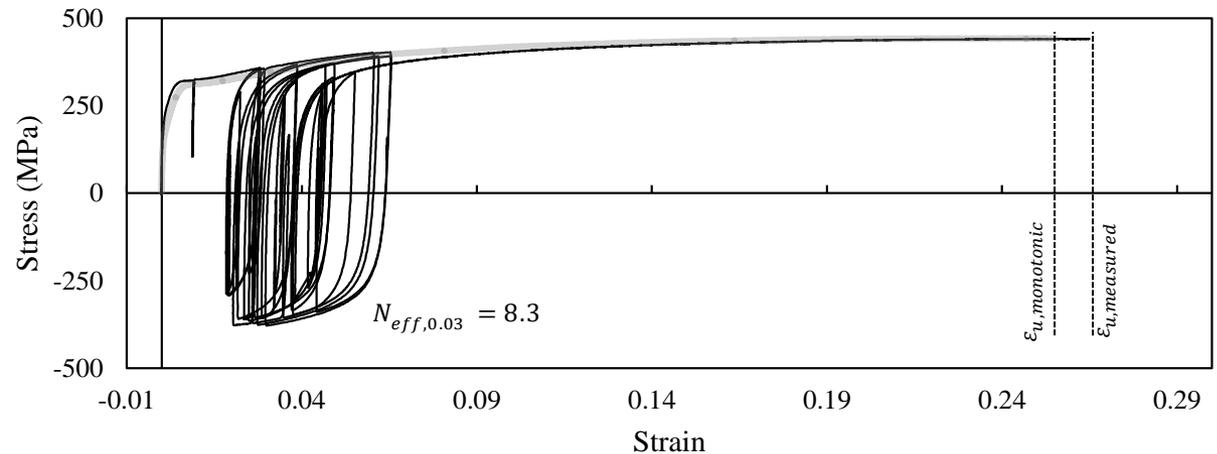
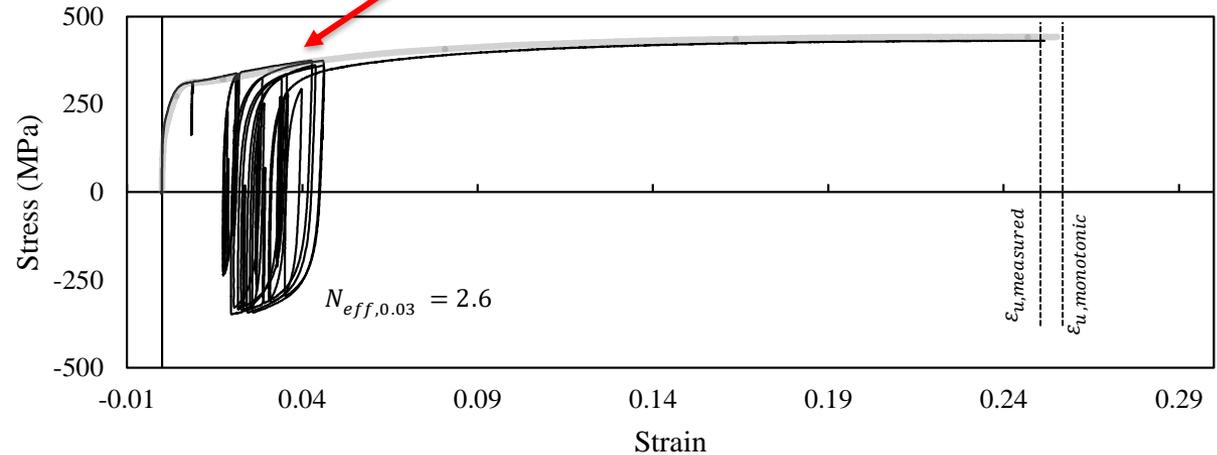
Figure taken from Ghannoum and Slavin (2016)

What about low-cycle fatigue?

Strain history measured on beam specimen during long duration earthquake loading

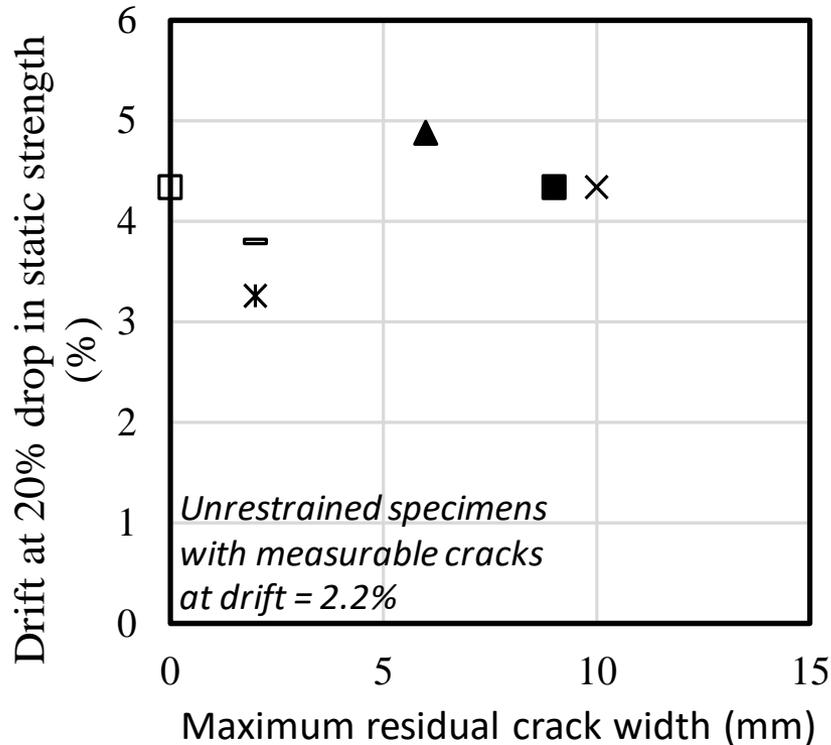


$4d_b$ clear span testing (300E)



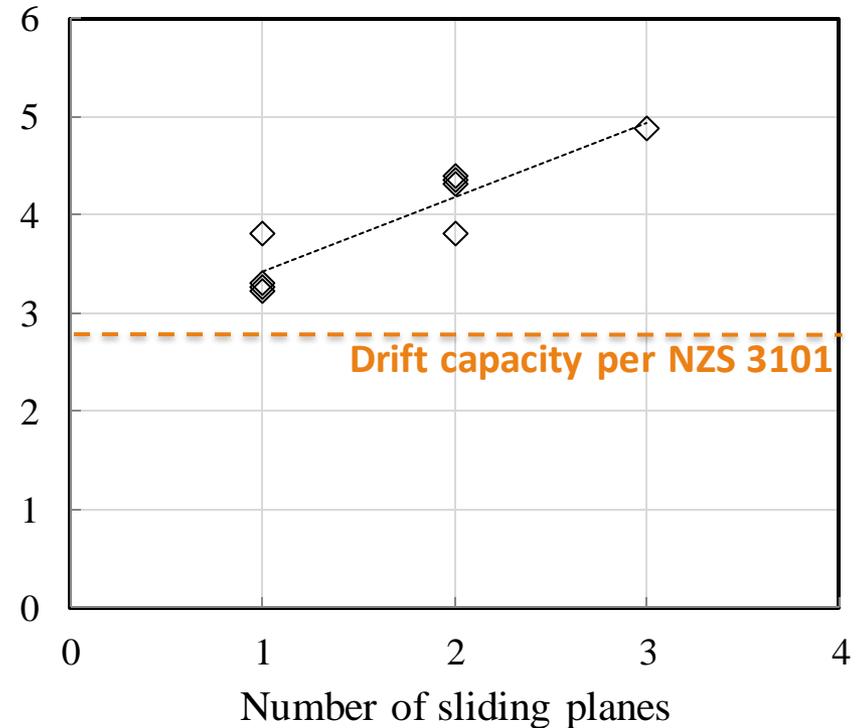
Damage → Drift capacity?

■ CYC ▲ P-1 × LD-1 * P-2 = P-2-S □ CYC-NOEQ



(after all cycles at or below 2.2% drift)

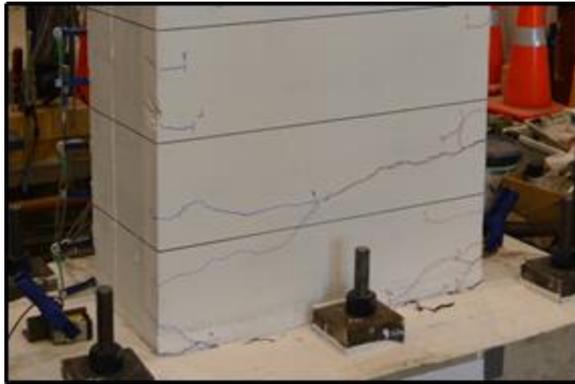
→ No relationship between crack widths and drift capacity.



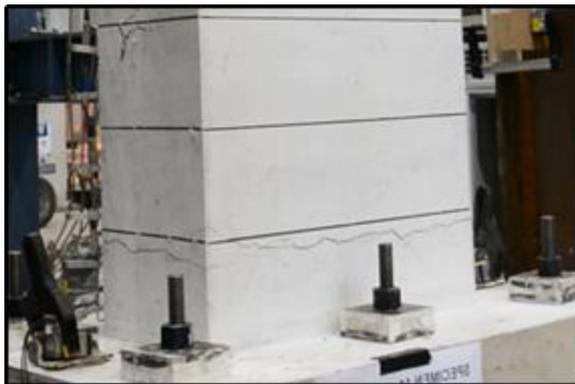
→ Drift capacity correlated with number of sliding planes.

Drift Capacity

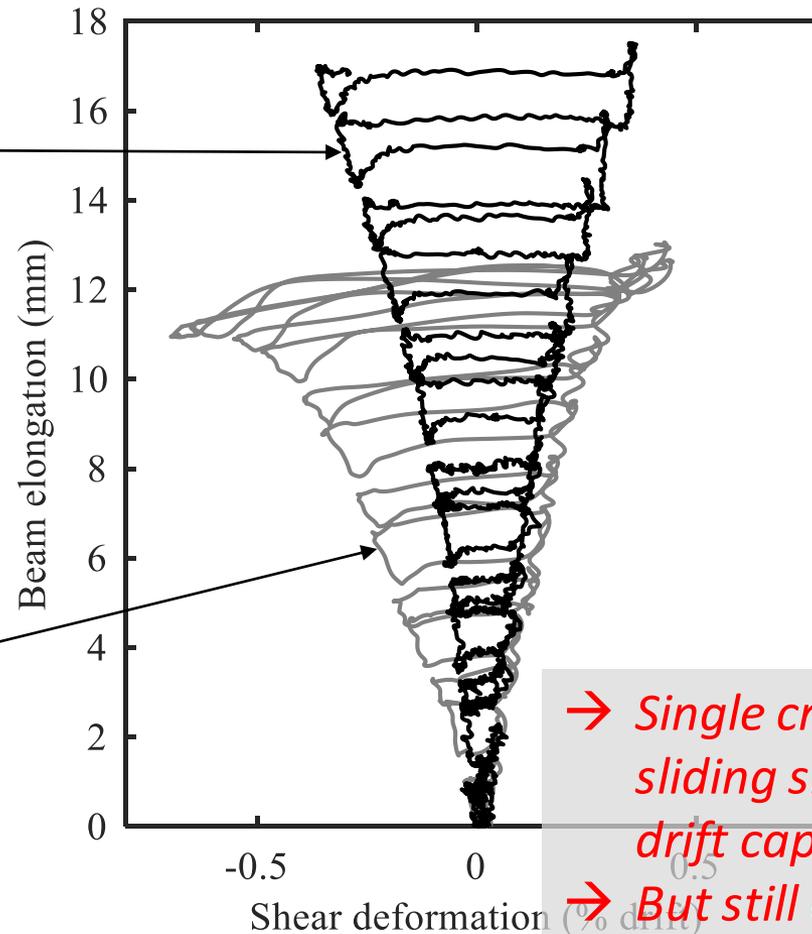
- limited by sliding shear



— CYC (multiple sliding planes)



— CYC-DYN (single sliding plane)



→ Single crack $w = 2-3\text{mm}$, sliding shear will limit drift capacity.

→ But still above NZS 3101 drift capacity.