Structural health monitoring data analysis on two cable stayed bridges in the UK & China

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Contents

- Background
- Temperature field analysis
- Traffic induced deflections
- Conclusions



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Background

Long-span bridges significance

- At critical locations, providing vital links
- High cost to construct and maintain
- Extensive social impact closure due to structural issues

Long-span bridges issues

- Ageing bridges 42% of bridges are 50+ years old in the US
- 7.5% of bridges are structurally deficient in the US
- Truss end link failure discovered on the Forth Road Bridge, Edinburgh, UK in 2015





Background

Project Ambition: Big Data & Data Centric Engineering: The Forth Bridges

Aim:

Develop this new holistic structural health monitoring SHM strategy on the Forth Bridges and then extend the research via the Yangtze River Bridge - towards the "International Living Bridge Laboratory" aci

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(a) The Queensferry Crossing in the UK (b) The Nanjing Dashengguan Yangtze River Bridge in China

- The NDB, formerly known as the Third Nanjing Yangtze River Bridge, opened in 2005
- Vital transportation link crossing the middle and lower Yangtze River & connecting Nanjing City and its Liuhe District.
- It is a double-steel-tower cable-stayed bridge with a main span of 648m.
- A unique feature of this bridge is its 215m-high arc-shaped steel tower first-of-kind among such long-span bridges.
- Superstructure deck: 3.2-m deep x 37.5-m wide orthotropic steel box girder 3 traffic lanes in each direction.

Background

Inspections

Visual Inspection

Structural Health Monitoring (SHM)

 Using periodically sampled response measurements to monitor changes to the material and geometric properties of engineering structures. Non-destructive Testing (NDT)

The difference between NDT and SHM is the sensors in the SHM systems are permanently installed on the structures to monitor environmental factors, external loadings and structural responses.

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| Structural health monitoring (SHM) Sensor Type | Queensferry Crossing | Forth Road Bridge |
|--|-------------------------|----------------------|
| Accelerometers | 102 | - |
| Air Temperature Sensors | 13 | 2 |
| Anemometer | 11 | 2 |
| Asphalt Temperature Sensors | 40 | 6 |
| Barometers | 2 | 1 |
| Bearing Gauges | 16 | 8 |
| Bearing Pressure Sensors | - | 8 |
| Concrete Deck Temperature Sensors | 70 | - |
| Concrete Tower Temperature Sensors | 46 | - |
| Corrosion Sensors | 360 | - |
| Displacement Transducers | 32 | 48 |
| Dynamic Weigh-in-Motion Sensors | 96 | 64 |
| GPS Location | 21 | 10 |
| Rainfall Gauges | 2 | 1 |
| Relative Humidity Sensors | 12 | 34 |
| Strain Gauges | 887 | 128 |
| Stay cable temperature sensors | 56 | - |
| Steel Surface Temperature Sensors | 158 | 32 |
| Main Suspension Cable Acoustic Monitoring | - | 116 |
| Tiltmeters | 48 | 16 |

Sensors on bridges

- Various original sampling rates (e.g. 1Hz, 10Hz)
- Recorded sampling rate: 1Hz
- Data size
 - FRB: 24GB/month
 - QC: 200GB+/month

| Number of sensors | Bridge |
|-------------------|-------------------|
| ~2,000 | Queensferry |
| ~192 | Forth Road Bridge |
| ~1,000 | Yangtze Bridge |



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Sensors layout



Sensors layout



Yangtze River Bridge

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Yangtze River Bridge – finite element model



Temperature field – concrete deck



Figure 6.12: Temperature features of the concrete deck

Temperature field – Tower temperature difference

QC: thermal centre tower

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Temperature difference (Max)

4.0 3.5 3.0 2.5 2.0 1.5 1.0 0.5 0.0 Jul Aug Sep Oct Nov Dec Jan Feb Mar Apr May Jun 2021 Time Distribution of temperature difference



Temperature field – Tower temperature difference

DDB: thermal centre tower







Extreme temperature estimation – GPD

The standard cumulative distribution function (CDF) of the GPD is defined by:

$$G(x; \sigma, \xi) = \begin{cases} 1 - (1 + \xi \frac{x}{\sigma})^{-1/\xi} & \text{for } \xi \neq 0\\ 1 - exp(-\frac{x}{\sigma}) & \text{for } \xi = 0 \end{cases}$$

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Calculate the mean excess

Calculate cumulative probability:

$$p=(1-P_r)^{1/N}$$

Calculate the extreme value
$$x_p$$

 $x_p = u_0 + \frac{\sigma}{\xi} \left[\left(\frac{n}{N_u} (1-p) \right)^{-\xi} - 1 \right]$

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$$e(u) = \frac{1}{N_u} \sum_{i=1}^{N_u} (x_i - u) = \frac{\xi}{1 - \xi} u + \frac{\sigma}{1 - \xi}$$

Plot the MEF Plot the mean excess e(u) against the threshold u. **Identify the threshold** In the GPD, the mean excess function is linear in the threshold for a suitable choice of threshold. The point where the plot starts to appear linear can be considered as a good threshold.

Extreme temperature estimation – Tower





(a) Inner & outer temperature difference on (b) MEF plot for tower temperature differcentre tower ence



Figure 6.23: Tower inner & outer temperature difference analysis

TOWER SECTION SCALE 1:100

- Estimated maximum temperature difference in 120 years is 4.66°C
- Not specified in Eurocode
- Chinese Design Code, 5°C

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Thermal-deflection relationship



- Displacements oscillate in a higher frequency compared to temperature
- High frequencies due to dynamic loads need to be separated from the signal

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Thermal-deflection relationship

Table 7.2: Thermal-induced deflection predictions data samples (part 1)

| Time | Sdeck_bottom (°C) | Sdeck_top (° <i>C</i>) | cabletem lowerend (°C) | cabletem upperend (°C) | Sdeck soffit (°C) |
|-------|----------------------|----------------------------|------------------------------|------------------------------|-------------------------|
| 15:10 | 14.505 | 14.971 | 13.778 | 15.845 | 14.304 |
| 15:20 | 14.505 | 14.978 | 14.003 | 15.875 | 14.327 |
| 15:30 | 14.510 | 14.988 | 14.250 | 15.894 | 14.367 |
| 15:40 | 14.520 | 15.001 | 14.347 | 15.901 | 14.408 |
| 15:50 | 14.535 | 15.016 | 14.565 | 15.958 | 14.464 |
| 16:00 | 14.555 | 15.032 | 14.429 | 15.990 | 14.488 |
| 16:10 | 14.571 | 15.049 | 13.931 | 15.982 | 14.453 |
| 16:20 | 14.574 | 15.063 | 13.601 | 15.935 | 14.391 |
| 16:30 | 14.565 | 15.075 | 13.538 | 15.854 | 14.328 |
| 16:40 | 14.547 | 15.084 | 13.338 | 15.772 | 14.254 |

Table 7.3: Thermal-induced deflection predictions data samples (Part 2)

| Time | cdeck_1 (° <i>C</i>) | cdeck_2 (° <i>C</i>) | cdeck_3 (° <i>C</i>) | cdeck_4 (° <i>C</i>) | cdeck_5 (° <i>C</i>) | GPS (mm) | gps wavelet (mm) |
|-------|--------------------------|--------------------------|--------------------------|--------------------------|--------------------------|-------------|------------------------|
| 15:10 | 16.575 | 15.564 | 14.728 | 14.460 | 14.266 | -0.065 | -1.734 |
| 15:20 | 16.595 | 15.583 | 14.754 | 14.469 | 14.263 | 0.343 | -1.603 |
| 15:30 | 16.606 | 15.602 | 14.779 | 14.480 | 14.297 | 4.730 | -1.542 |
| 15:40 | 16.611 | 15.620 | 14.803 | 14.492 | 14.346 | -2.684 | -1.526 |
| 15:50 | 16.614 | 15.637 | 14.825 | 14.506 | 14.397 | 3.921 | -1.526 |
| 16:00 | 16.617 | 15.657 | 14.846 | 14.522 | 14.429 | -3.585 | -1.521 |
| 16:10 | 16.618 | 15.674 | 14.867 | 14.540 | 14.390 | -1.843 | -1.491 |
| 16:20 | 16.610 | 15.691 | 14.887 | 14.558 | 14.307 | 1.209 | -1.419 |
| 16:30 | 16.583 | 15.707 | 14.907 | 14.575 | 14.247 | -10.630 | -1.285 |
| 16:40 | 16.532 | 15.722 | 14.926 | 14.590 | 14.180 | -9.717 | -1.071 |



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Queensferry Crossing traffic flow











- 2 GPS stations installed at the south midspan
- The simulated deflections show similar pattern as the monitored data



Traffic induced deflections – predictions



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Conclusions

- Temperature difference should be considered in the analysis for concrete sections
- Extreme temperature difference analysis reveals that the extreme estimation for bridge tower thermal load is close to the Chinese Design code - A revision of Eurocode in this part should be considered.
- LSTM is efficient in mapping the relationship between traffic attributes and deck deflections - In practical use, the model can be first trained on simulated data and then calculate the actual deflections at any locations of interest by being provided with real WIM data.
- LSTM demonstrates robust predictive capability on temperature-deflection relations even with time lag between them.

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